



Labyrinth Gold Project, Canada

Initial Inferred Mineral Resource of 500,000oz at 5g/t sets up Labyrinth as significant high-grade project

Outstanding potential for further growth with Resource open in all directions and high-grade mineralisation already intersected well outside the Resource boundaries

Key Points

- Initial Inferred Mineral Resource of 3 Mt @ 5.0 g/t Au for 500,000 oz (at 3 g/t.m cut-off)
- Mineral Resource prepared by an independent Competent Person and classified and reported in accordance with the JORC Code (2012)
- Notable high-grade component of 150,000 oz at 10 g/t (above 6 g/t cut-off)
- Mineral Resource for the key Boucher Lode totals 1 Mt @ 5.7 g/t for 190,000 oz and remains open along strike and at depth
- The estimate is based on an extensive drilling database and rigorous modelling by independent consultants RSC
- The Mineral Resource exceeds the foreign estimate of 479,000 oz published in 2010¹
- The Resource is open in all directions, supporting substantial Mineral Resource growth potential through both near-mine and regional drilling
- The growth potential is supported by numerous recent high-grade intersections outside the Mineral Resource extent; these include 1.4 m @ 13.32 g/t, incl 0.9 m @ 20.53 g/t, in LABS 22-02 and 2.9 m @ 5.63 g/t, incl 0.9 m @ 7.9 g/t, in LABS 22-04²
- This extensive known mineralisation provides a pathway to significant, rapid growth in the Resource
- Strong project outlook also underpinned by exceptional metallurgical results, with an initial bulk-leach extractable gold (BLEG) test returning 97.1% recovery
- BLEG result demonstrates that the material is free milling, which would significantly reduce capital and operating costs of any potential future operation

Next Steps:

- Planning underway for new drilling campaign with the aim of bringing known mineralisation into the Mineral Resource
- Finalise regional drilling targets across the broad Labyrinth tenure, with specific focus on the strike extension of the highest-grade Boucher lode at the projected intersection point of the hosting Labyrinth Fault and the gold-mineralised Hunter Creek Fault
- Detailed interrogation of the resource model will be undertaken to define near-mine high-grade opportunities around the existing five levels of the underground mine

¹ Refer to ASX Announcement 2 September 2021

² Refer to ASX Announcement 24 August 2022



Labyrinth Resources Limited (ASX: LRL) is pleased to announce an initial Inferred Mineral Resource of 3 Mt @ 5.0 g/t Au for 500,000 oz at its Labyrinth Gold Project in Quebec, Canada.

The Mineral Resource was prepared by a Competent Person and classified and reported in accordance with the JORC Code (2012).

The Labyrinth project is situated within the prolific Abitibi Greenstone Belt and has been historically mined, most recently in the 1980s.

The Company rapidly progressed ~7,800 m of underground and surface diamond drilling to facilitate the conversion of the Project's foreign estimate (reported under NI 43-101 in 2010) into a Mineral Resource reported in accordance with the JORC Code (2012).

The Inferred Mineral Resource includes mineralisation within five lodes: Boucher, McDowell, Talus, Shaft and Front West (Table 1). In addition to the known mineralisation, there is also immense potential to grow the Mineral Resource given that the key lodes remain open along strike and at depth (Figure 1).

Several of the recently reported high-grade results² from the surface drilling campaign fall outside of the Inferred Mineral Resource reported here, due to the drill spacing, indicating the immediate potential for scale increases following infill and step-out drilling.

Labyrinth Chief Executive Matt Nixon said: *"This is a very strong initial Mineral Resource which lays the foundations for ongoing resource growth.*

We have exceeded the foreign estimate (reported under NI 43-101 in 2010¹) with our first campaign and in the process shown that Labyrinth has genuine scale with an outstanding grade of 5.0 g/t.

In addition to the Resource, drilling has established significant high-grade mineralisation which remains open at depth and along strike, paving the way for strong growth in the resource.

Drilling will now target this mineralisation to bring it into the Resource while also testing a host of regional targets.

We are confident that given the additional mineralisation we have already identified and the fact that it is open in all directions, ongoing drilling will drive the Resource and create substantial shareholder value over coming months".

Table 1 – Labyrinth Inferred Mineral Resource.

	Lode	Tonnes (Mt)	Au (g/t)	Au (oz)
Inferred	Boucher	1	5.7	190,000
	McDowell	1	4.5	150,000
	Talus	0.7	5.3	110,000
	Front West	0.2	2.7	20,000
	Shaft	0.1	5.5	30,000
	Total	3	5.0	500,000

Notes:

1. Reported at a 3 g/t.m accumulation (grade x vein thickness) cut-off and depleted for historical mining.
2. The Mineral Resource is classified in accordance with the JORC Code (2012).
3. The effective date of the Mineral Resource estimate is 25 August 2022.
4. Estimates are rounded to reflect the level of confidence in the Mineral Resource at present. All resource tonnages have been rounded to the first significant figure. Differences may occur in totals due to rounding.
5. Mineral Resource is reported as a global resource.

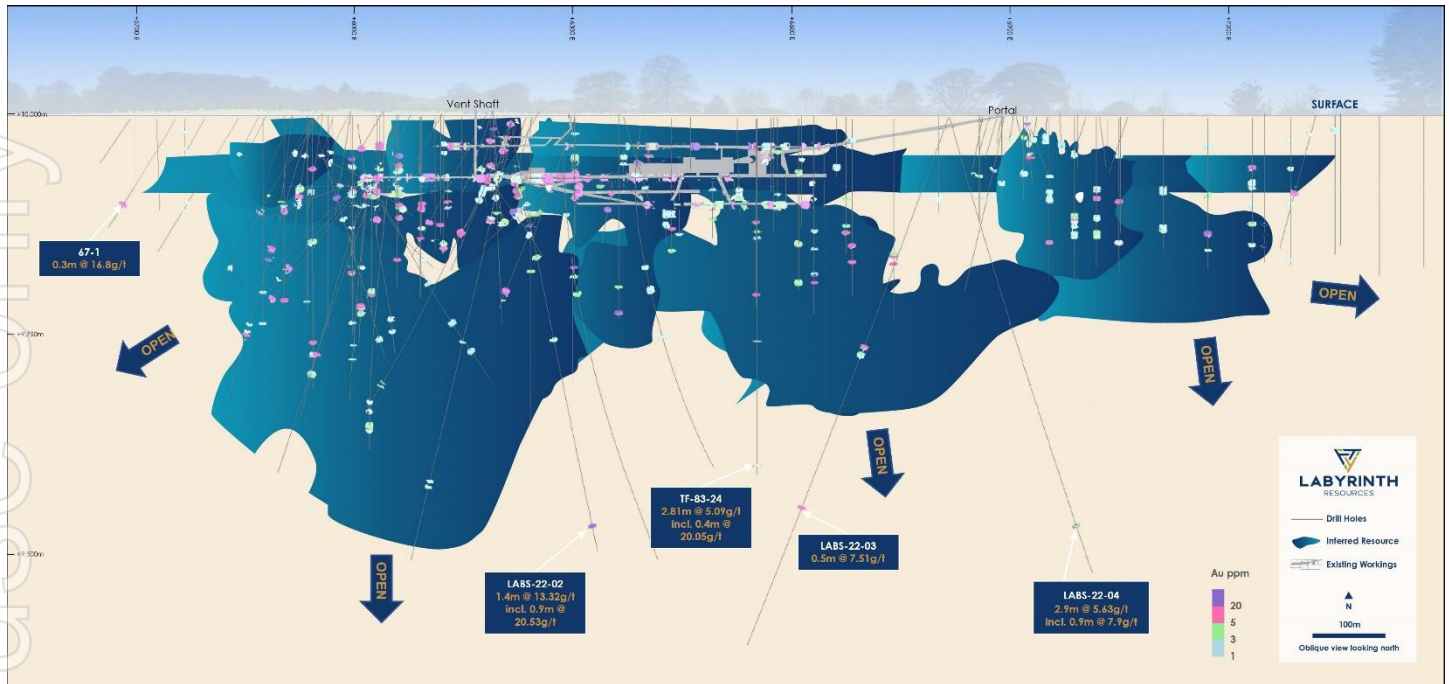


Figure 1 – Long section of Labyrinth Inferred Mineral Resource and drilling results.

The model comprises four lodes within the Main-lode system of the historical mine (McDowell, Talus, Shaft and Front West; Figure 2). The Main-lode model extends 1.7 km along a strike of 080 and dips $\sim 60^\circ$ to the south. The less-explored Boucher lode system is situated to the north of the Main-lode and was modelled separately. The Boucher lode consists of several parallel mineralised veins with a strike of 060 and dipping $\sim 65^\circ$ towards the southeast. The Boucher system was modelled over 1 km of strike (Figure 2). Veins within the Boucher lode exhibit higher grades overall than the Main-lode structures (Table 1).

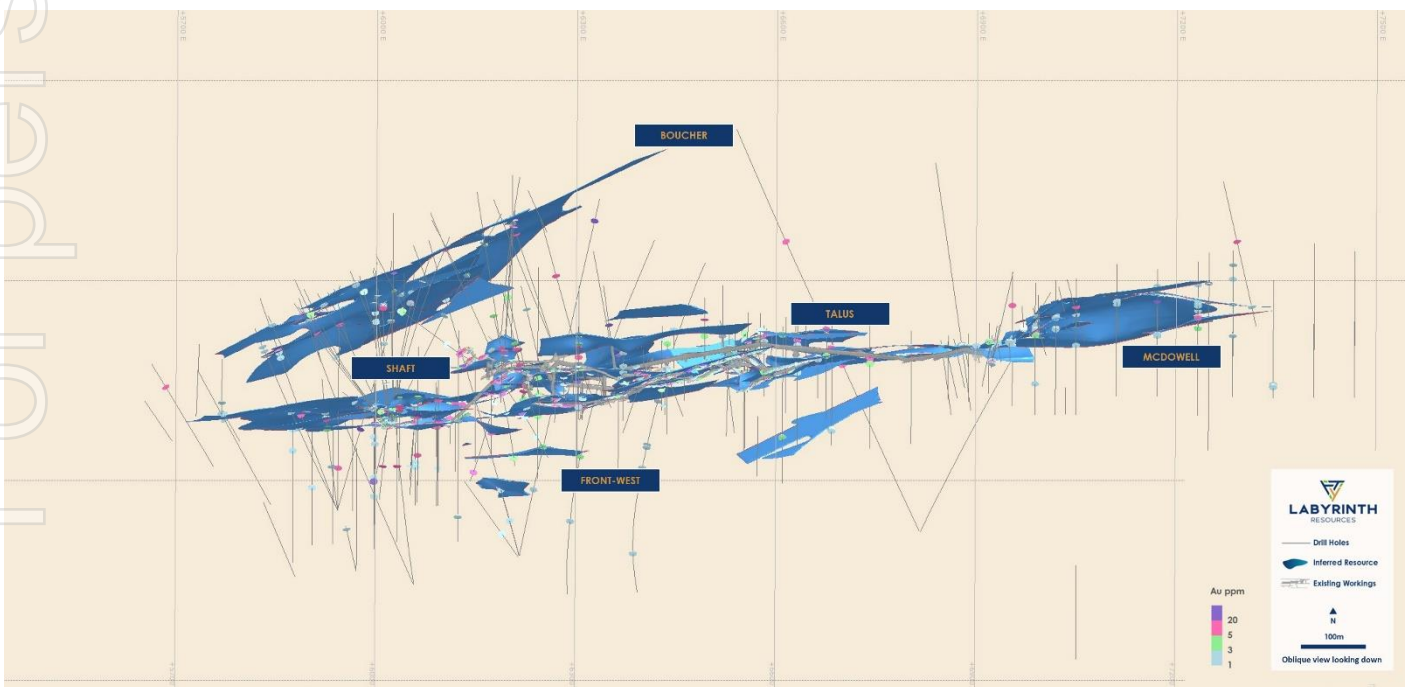


Figure 2 – Plan Map of lodes within the Labyrinth Mineral Resource.



The high-grade component of the Labyrinth Mineral Resource is presented at various Au cut-off grades in Table 2.

Table 2 – Total Mineral Resource at various Au cut-off grades demonstrating significant high-grade component.

	Au cut-off (g/t)	Tonnes (Mt)	Au (g/t)	Au (oz)
Inferred	2	3.0	5.0	500,000
	4	1.5	6.5	300,000
	6	0.5	10	150,000
	8	0.3	12	100,000
	10	0.2	14	90,000

Notes:

1. Reported at various Au cut-off grades as specified and a minimum vein thickness of 1.5 m, ie the 2g/t cut-off grade is reported at a 3 g/t.m accumulation (grade x vein thickness) cut-off and depleted for historical mining.
2. Differences may occur in totals due to rounding

Metallurgical Test Work

Recent preliminary metallurgical testing has returned exceptionally high recoveries from Bulk Leach Extractable Gold (BLEG).

The test work was based on 35 mineralised samples, composited into a master 40 kg bulk sample, collected from recent diamond drilling at Labyrinth. The samples were collected from five holes. Samples were processed at Base Metallurgical Laboratories (Baselab) and managed by JT Metallurgical Services. Processing to date has involved comminution and gold extraction by conventional gravity and cyanide leach gold recovery and by bulk leach extraction.

BLEG is a cyanide-based partial leach procedure carried out on large samples to assess the absolute highest recovery possible via cyanidation. A 1 kg composite ground to P80 <20 µm returned a BLEG recovery of 97.1% (Table 3). This illustrates the gold is not refractory and supports the potential of leaching a flotation concentrate onsite.

Initial tests on a 20 kg sample of the master composite by gravity concentration followed by intensive leach demonstrated gold recovery of 92.2% for the Knelson concentrate (Table 4).

The Baselab team is now proceeding with additional leach tests and rougher flotation tests on the gravity tail.

Table 3 – Bulk Leach Extractable Gold recoveries from Labyrinth composite test.

Sample size	Grind size (µm)	Feed grade	Au extraction (%)	Au tail (g/t)
1 kg	20	5.6	97.1	0.17

Table 4 – Gravity and combined gravity + leach recoveries from Labyrinth composite test.

Master Composite Gravity Concentration					Intensive Leach on Gravity Concentrate		
Sample size	Grind size (µm)	Feed grade	Recovered head grade	Gravity recovery (%)	Au extraction (%)	Au tail (g/t)	Gravity Recovery to Dore (%)
20 kg	300	4.1	5.7	15.6	92.2	12.6	14.4



This announcement has been authorised and approved for release by the Board.

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In compliance with the ASX Listing Rules 5.8.1 for the public reporting of a Mineral Resource, the Company provides the following information.

GEOLOGY AND GEOLOGICAL INTERPRETATION

Regional Geology

The Labyrinth Project is located in the southeast of the Superior Province, which forms the heart of the Canadian Shield and consists of a series of Late Archean terranes (Figure 3). The Project is situated in the centre of the volcano-plutonic Abitibi subprovince, specifically the Abitibi Greenstone Belt (AGB).

The AGB consists of east-trending successions of folded volcanic and sedimentary rocks and intervening domes of intrusive rocks, including the volcanic rocks of Blake River Group (BRG), which host the Labyrinth deposit. Rocks of the BRG are located between the east-west Destor-Porcupine-Manneville Shear Zone (DPMSZ) and Cadillac-Larder Lake Shear Zone (CLLSZ) which are host to several major orogenic gold deposits.

BRG volcanic rocks are predominantly bimodal in composition (basalt – basaltic andesite – andesite versus rhyodacite – rhyolite). Archean syn-volcanic (gabbro, diorite, tonalite) and syntectonic intrusions (syenite, diorite, granodiorite, granite), and Proterozoic gabbro dykes (diabase) cut the BRG volcanic rocks.

Project Geology

Lithologies encountered within the Labyrinth Project are rhyolites and andesites of the Noranda Complex, BRG, cut by pre- and syn-tectonic masses of intrusives of gabbroic-dioritic composition. The contact between the intrusive and the andesite is characterized by the presence of a shear zone and associated with deformed and boudinaged quartz veins. The shear zones hosting Labyrinth are regionally continuous on kilometre-scale with a local-scale anastomosing nature meaning splays and vein intersections are common.

The hanging wall consists of mafic flows, felsic porphyry and interlayered diabase and gabbro. The footwall consists of andesite. The hanging wall mafic flows are variably greenschist altered, although the most discernable and strongly altered sections are immediately above the lower bounding fault. The expression of this structural contact is variable.

A variably altered pink felsic porphyry is in contact with the base of the mafic flows in several holes. The lower contact has been observed as having gradational to fault-bound control, which in some cases is mineralised. Beneath the porphyry is a wide interval of interlayered diabase, gabbro, diorite and granodiorite. The gabbro hosts up to 10% magnetite and ilmenite. Alteration across this unit occurs near sheared intervals and is marked by chlorite, leucoxene, and carbonate along deformed quartz-carbonate veins. At the lower contact of the gabbro is a strongly chloritised,



sheared interval, with banded yellow-green sericite along the foliation and abundant deformed quartz-carbonate veins. This zone is variably mineralized with fine- and coarse-grained sulphides.

Below this shear zone is the andesitic volcanic unit. Minor amounts of sulphide (Trace to 5% pyrite, <1% chalcopyrite) as stringers and dissemination fill amygdules and fractures.

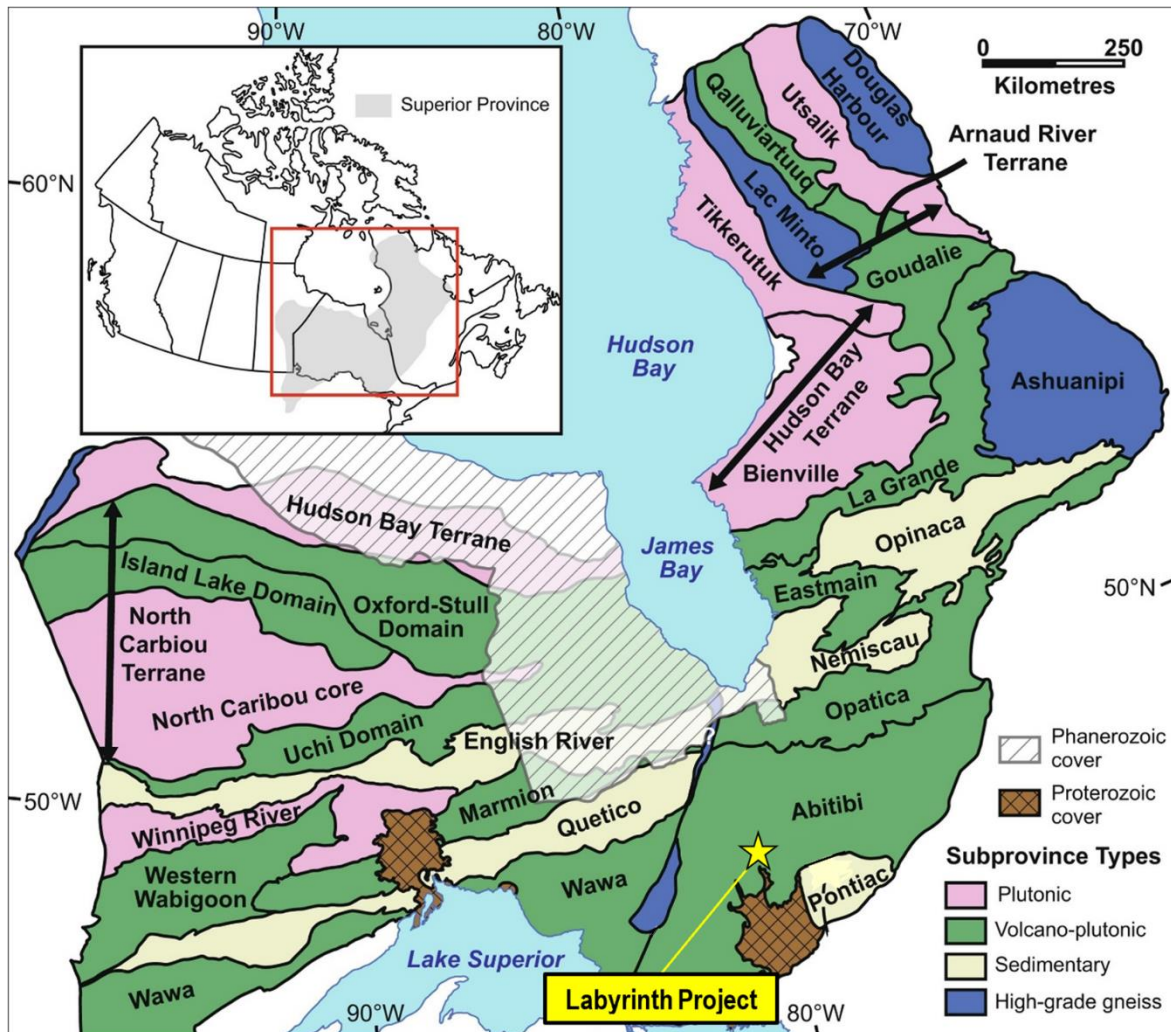


Figure 3 – Location of the Labyrinth Project within the Superior Province.

Controls on Mineralisation

Mineralisation consists of sulphide-rich quartz-carbonate veins within discrete shear zones and is typically associated with a sericite-chlorite-leucoxene alteration package. The shear zones usually host bands of mm to m wide foliation (sub)parallel quartz-carbonate veins and stringers that in some cases carry visible gold. Sulphide mineralisation present is almost exclusively pyrite, but trace arsenopyrite and chalcopyrite have been observed. Sulphide mineralisation typically occurs as semi-massive and massive pyrite stringers and grey-quartz hosted finely disseminated pyrite. Bands of higher pyrite content often occur at vein margins where wall rock is strongly altered.

Mineralisation is predominantly hosted in east-west trending quartz veins within the altered and sheared diorite and andesite. Orientations of the mineral-bearing structures vary from N070° to N090° with dips ranging between 55° and 80° towards the south. Quartz veins can in places be traced for at least 1.4 km along strike. Mineralisation is crosscut in several places by transverse faults with weak displacements.



DRILLING TECHNIQUES

The Labyrinth Mineral resource estimate has been informed by data from diamond drilling conducted by Labyrinth Resources in 2022 and legacy explorers. Historical channel samples (449) and level plans have also informed the estimate. The data cut-off for the Mineral Resource estimate is 25 August 2022. The drilling database includes results from 17 underground holes (~4,700m) and five surface holes (~3,100 m) drilled by Labyrinth and 239 legacy holes. The drillhole spacing is highly variable but is typically 40–80 m.

2022

Labyrinth's 2022 underground drilling programme was conducted using an LM90 drill rig with wireline core barrel recovery through the inside of the drill string and employing either an NTW (3 holes) or BQ (14 holes) sized diamond drill bit at the face. The holes were drilled approximately perpendicular to the strike of mineralised structures at various dips (45–57°) to intercept close to true mineralisation widths. The average hole length was 277 m. Core recovery at the rig was measured by contract geologists from Gold Minds Geoservices and was good (average >95%). The geologists communicated with the driller when recovery issues were identified, and the driller used different mud and drilled more carefully to maximise recovery in these zones. Holes were collared within several historical underground drives on an ~80 m hole spacing within each drive.

Labyrinth's surface drilling used a skid-mounted diamond drill rig with wireline core barrel recovery through the inside of the drill string and employed an NQ-size diamond drill bit at the face. The five holes were drilled approximately perpendicular to the strike of mineralised structures at various dips (60–70°) to intercept close to true mineralisation widths. The average hole length was 620 m. Drillhole spacing was variable as the programme was designed to test the continuity and extent of the Main-ode. Core recovery at the rig was measured by contract geologists from Mercator Geological Services and was good (average >95%).

Historical

Between the initial discovery in 1924 and 1986, at least 23,200 m across 166 diamond BQ-sized holes were drilled. Unverified historical drillholes and holes with poor core recovery logs have not been incorporated into the project database compiled by SGS. Specific details of the historical drilling procedures are unknown. Holes were drilled at various orientations and dips, however, most holes were oriented approximately north with dips between 45° and 70°. Two series of vertical holes were drilled in 1952 and 1983. The average hole length was 140 m.

No further drilling was conducted between 1986 and 2005.

From 2006 to 2010, Rocmec Mining Inc (Rocmec) drilled approximately 12,300 m over several surface and underground campaigns.

The Rocmec 2006 surface drilling campaign totalled 1,900 m from three diamond holes. The programme was managed by a drilling contractor for Rocmec using BQ size core and metric drill rods.

The 2007 surface drilling totalled 1,000 m over four ATW-sized diamond holes.

The Rocmec 2006–2009 underground drilling campaign was done by Rocmec with its own rig using BQ size core and imperial drill rods. A total of 47 holes were drilled for 3,900 m.

The Rocmec 2009 surface drilling campaign was done by Forage Rouiller of Amos using NQ size core and metric drill rods. Drill supervision was done by SGS of Blainville, Quebec. A total of 5 holes were drilled for 2,000 m.

The Rocmec 2010 surface drilling campaign was done by DCB Drilling of Rouyn-Noranda using NQ size core and metric drill rods. A total of 14 holes were drilled for 2,000 m. SGS was responsible for drill supervision.



SAMPLING AND SUB-SAMPLING TECHNIQUES

Sampling

2022

Sampling by Labyrinth during the 2022 diamond drilling programmes was undertaken using NTW (61.5 mm) or BQ core (36.5 mm) for underground holes and NQ core (50.7 mm) for surface holes. Core recovery was recorded during drilling and was excellent throughout the programmes (>95%). Core was meter-marked and geologically logged prior to marking for sampling. Sample-marked core was photographed. Where possible core samples were taken at 1 m intervals, however, variable shorter lengths were taken at geological boundaries to a minimum of 30 cm. Density testing was also undertaken at this stage prior to crushing and splitting. The density of the 2022 core was measured using an 'Archimedes' type water displacement method. However, the method used results in a minor sample selection bias towards long competent pieces of core.

Pre-2006

Samples between 1924 and 2006 were collected as BQ core. The specifics of the sampling procedures, including quality assurance and quality control, are unknown. However, it appears that the whole core was sampled from mineralised intervals on nominal 0.5 m intervals or as defined by the visual presence of mineralisation. The unmineralised core was discarded. Available records suggest variable core recovery.

2006–2010

Samples from the 2006 surface, 2006–2007 underground and 2008–2009 underground drilling were collected as BQ core. Records show upwards of 90% recovery. Samples were taken following logging on nominal 0.5 m intervals or as defined by geological boundaries determined by the logging geologist or technician. Records show upwards of 90% core recovery.

Samples from the 2007 surface drilling were collected as ATW core. Rocmec technicians sampled the entire mineralised core intervals on nominal 0.5 m intervals or as defined by geological boundaries.

NQ core samples were collected during the 2009 and 2010 surface drilling campaigns. Samples were collected by SGS following logging. Records show upwards of 90% core recovery.

Channel samples were also collected between 2006 and 2009; however, specific sampling procedures used are unknown.

Sample Preparation

2022

NTW core was half cut using a diamond table saw. One side of the core was consistently taken to ensure no bias is introduced when sampling. NTW half-core samples and BQ whole-core samples were sent to Sawslabs for preparation and assay. Samples were crushed to >80% passing 1700 microns using low chrome steel jaw plates, split using a rotary splitter, pulverised to >85% passing 74 microns, homogenised and split into 30 g pulp samples for assay using a spoon. No duplicates were collected during the sample preparation process to monitor the data quality.

Samples containing visible gold were analysed by a screen fire assaying method, consisting of them being sieved after splitting to remove the coarse fraction.

Pre-2006

Sample preparation procedures are unknown. No records of QC data are available for the sample preparation process.



2006–2009 BQ & ATW Samples

Whole-core BQ and ATW samples were sent to Expert Laboratory of Rouyn-Noranda for sample preparation and analysis. The laboratory was not certified; however, its personnel followed strict written procedures for the preparation and analysis of the samples. Once received by the lab, the primary samples were dried and crushed to -1/4 inch with a jaw crusher. Samples were reduced to 90% passing -10 mesh with a rolls crusher. The first sample of each batch was screened by the lab to verify that 90% passed 10 mesh. Samples were split using a Jones-type riffle splitter to obtain a 300 g sub-sample which was pulverised to 90% passing -200 mesh using a ring and puck-type pulveriser. The first sample of each batch was screened by the lab to verify that 90% passed 200 mesh. A final sample weight of 29.166 g was weighed out into a crucible. RSC reviewed the available first-split (half core) duplicate data and considers the precision and accuracy of the first split to be acceptable for classifying an Inferred Mineral Resource. No further records of QC data are available for the sample preparation process.

2009–2010 NQ Samples

NQ core was sawn into half-core samples which were sent to SGS Lakefield Laboratory for sample preparation and assaying. Samples were dried before crushing using primary and secondary crushers to achieve 85% passing 10 mesh. The laboratory checked one sample in 50 for % passing at the crushing stage. Samples were then split using a 12-slot, 1/2 inch splitter that divided the sample into two portions (pulp and reject). A representative head sample of -150 g was riffled and pulverised to obtain approximately 30 g of 150 mesh from the bulk sample. One replicate sample in every 20 samples was prepared. RSC reviewed the available pulp duplicate data pairs and considers the precision and accuracy of the third split (pulp) duplicates to be acceptable for classifying an Inferred Mineral Resource. No further records of QC data are available for the sample preparation process.

Sample Analysis Method

2022

The 2022 drilling samples were assayed for Au at Swastika Laboratories Ltd (SwasLabs) in Swastika, Ontario using method code FA-AAS. Samples were fire-assayed using a 30 g charge with an AAS finish. For the samples containing visible gold (with the coarse fraction removed), a weighted average method was used to determine the final assay grade.

Samples returning grades >10 g/t Au by AAS finish were reanalysed using method code FA-GRAV, which uses a gravimetric finish.

A quality control programme was maintained throughout the sample analysis. In addition to SwasLab's internal use of CRM material, Labyrinth's contract geologists inserted blanks and CRMs. These were inserted into the sample stream every 20th sample. Several different CRMs were used.

Labyrinth and the lab monitored internal CRMs results for consistency and checked for bias against certified values. RSC's review of CRM performance concluded that any observed bias was statistically insignificant (<2%) and that the analytical process delivered acceptable results. Blank results were monitored and confirmed no contamination at the laboratory.

Pre-2006

Sample assay methods are unknown.



2006–2009 BQ & ATW Samples

Samples were fire assayed with a gravimetric finish at Expert Laboratory of Rouyn-Noranda. The laboratory was not certified. However, its personnel followed written procedures for the analysis of the samples. The lower detection limit was 0.03 g/t. All values >3 g/t were verified before reporting.

Only laboratory quality control monitoring was used. Each furnace batch comprised 28 samples, including a laboratory inserted reagent blank and standard which were reviewed by the laboratory to ensure consistency. Standards were checked for bias.

2009–2010 NQ Samples

Samples were analysed for Au by metallic screen fire assay using a 30 g sample charge at SGS Lakefield, an accredited laboratory. Only laboratory quality control monitoring was used and the records are unavailable.

ESTIMATION METHODOLOGY

Geological Domains

Five major geological domains were created using implicit modelling workflows and based on downhole lithological logging data from Labyrinth and legacy drilling campaigns (diabase, diorite, felsic porphyry, andesite and overburden). The basal contact of the modelled overburden unit provided the first-pass constraint for mineralisation. The geological domain model was intersected by a fault model based on four fault planes interpreted from the offset of mineralisation observed in channel samples and legacy level plans. This resulted in the creation of a sixth geological domain, fault breccia.

Estimation Domains

A review of gold distributions within the geological domains demonstrates multimodality of gold grades symptomatic of a mixing of grade distributions within each domain. Geological domains are thus not at sufficient resolution to identify grade populations amenable to unbiased estimation. Estimation domains were created implicitly from gold grade data, which are considered to be a proxy for the quartz veining that hosts the mineralisation.

Wireframes for the estimation domains, representing the quartz veins, were created using an interval selection approach based on Au grade and guided by a numeric interpolant model using trends of Au mineralisation observed in the level plans to guide the search anisotropy. Mineralised intervals were selected from composited Au intervals with a minimum length of 0.5 m and a cut-off grade of 0.5 ppm. Where gaps remained in the estimation domain wireframes, individual grades ≥ 0.1 ppm were selected. Wireframes were not extended through barren/waste drillhole intervals, wireframes were snapped to drillhole contacts and were typically closed off halfway between a mineralised and an unmineralised interval in a drillhole.

Two vein systems were modelled; the Main-lode and Boucher. The Main-lode has a mean strike of 080 and dips $\sim 60^\circ$ towards the south, while the Boucher system strikes 060 and dips $\sim 65^\circ$ towards the southeast. Mineralisation of the Boucher system is spatially associated with the northeast trending andesite contact. Mineralisation within the Main-lode is spatially associated with the contacts of the felsic porphyry unit.

Mineralisation of the Boucher and Main-lode system remains open to the east, west and at depth. Estimation domains were initially extrapolated up to 400 m beyond mineralised intercepts and were not constrained during the estimation. However, the risk of extrapolation was considered when classifying and reporting the Mineral Resource by using a buffer of 80 m around existing drillholes.

The buffer was determined from a review of geological and grade continuity along strike and at depth.

Histograms of the composited grade assay data still identified the presence of a bimodal Au grade population in the Main-lode. After reviewing the spatial distribution of the high grades in 3-D in conjunction with probability density plots and downhole plots, high and low-grade domains were created for the Main-lode with CVs of 1.0 and 2.1, respectively. The Main-lode domains display a positively skewed population and this was taken into account when selecting the grade estimation method for the Main-lode domains. Basic stationarity checks were carried out for the high-grade and low-grade domains and reveal no major grade trends could be observed along strike or down dip.

The coefficient of variation for the composited data in the Boucher domain is 3.4 uncapped and 2.0 after grade-capping three samples to 60 ppm. No further distinction was made within the Boucher domain (i.e., no sub-domains were generated) as the grade population reveals no major grade trends could be observed along strike or down dip.

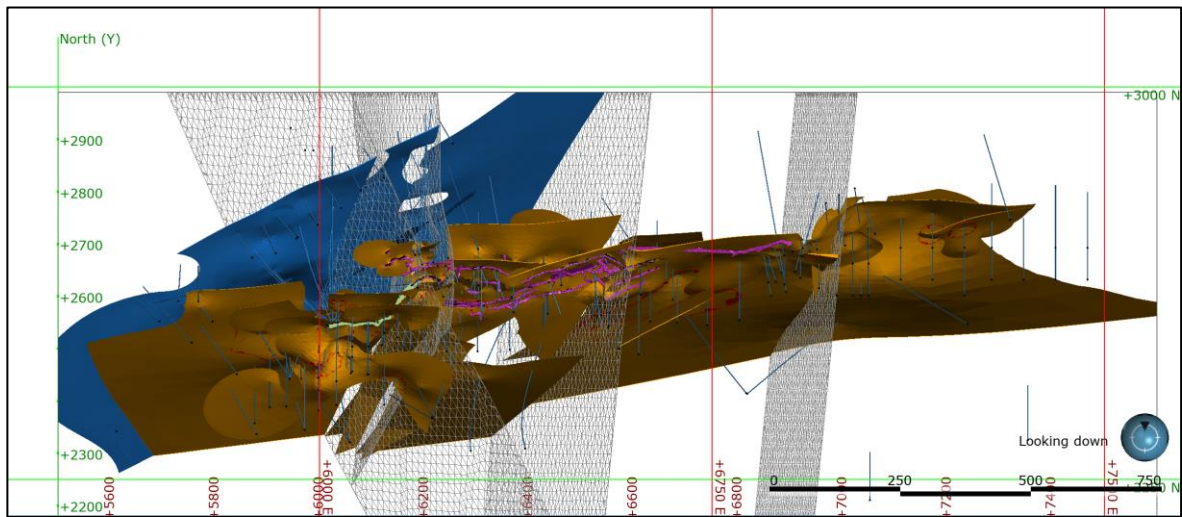


Figure 4 – Plan view of the Main-lode (orange) and Boucher (blue) estimation domains.

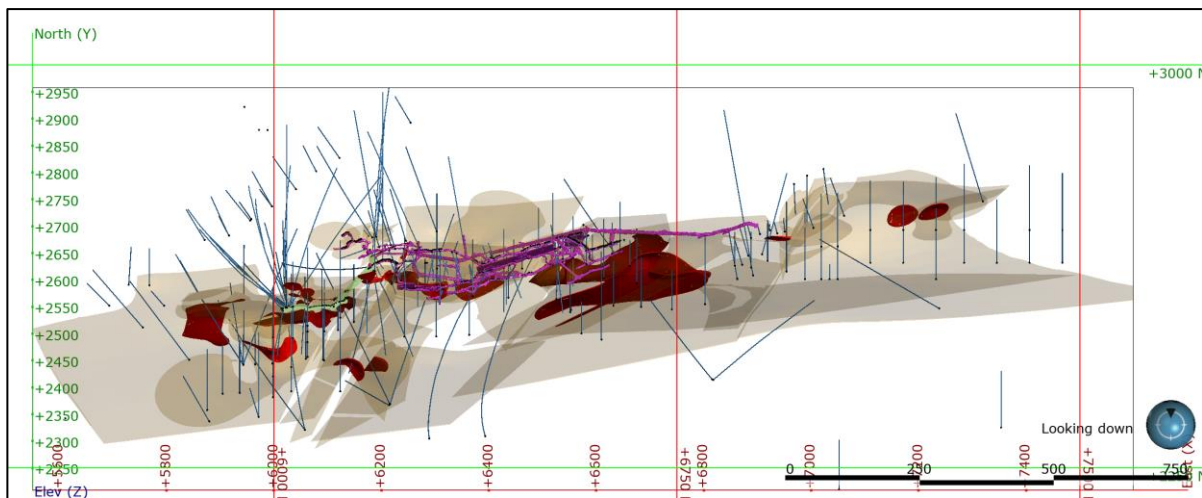


Figure 5 – Plan view of the Main-lode high-grade (red) and low-grade (transparent orange) estimation domains.

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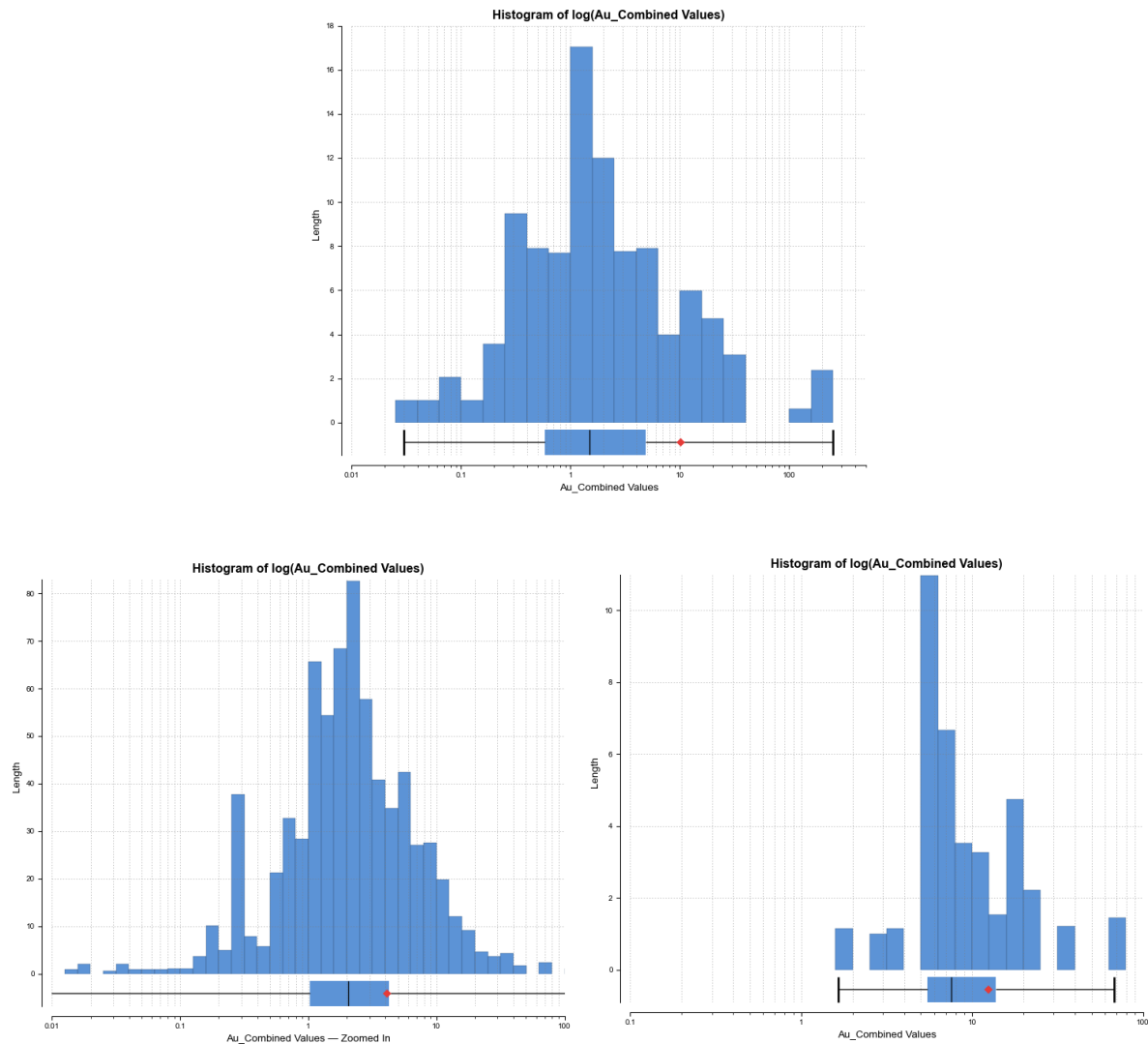


Figure 6 - Log histograms of Au within the Boucher (top), Main-lode LG (bottom left) and Main-Lode HG (bottom right) estimation domains.

Resource Estimation

Assay data were composited within estimation domains to 1 m intervals, a multiple of the dominant sample length of 0.5 m providing a smoothing effect on grade distributions. Residual intervals of less than 0.5 m were distributed evenly across the composites, and minimum coverage of 50% was applied.

Grade capping was necessary to lower the influence of outliers within the Boucher estimation domains. Grade capping to 60 ppm was applied after reviewing histograms and log probability plots. Distance-buffered grade capping was used to lessen the effect of top cutting locally.

The resource was estimated using ordinary kriging ('OK') for the Boucher domain and a top-cut with indicator residual methodology (Rivoirard et al., 2010) for the Main-lode domains. Au grades within the Boucher and Main-lode domains were estimated separately with the grades of one not influencing the grades of the other.

The top-cut with indicator residual method (Rivoirard et al., 2010) is adapted to estimating grade from very skewed distributions. This method splits the modelled grade distributions into two parts: the first part is the background distribution, characterised by the grade values cut to the top-cut threshold ('TC') and the second part is the tail of high-grade values characterised by the indicator

function at that threshold, $I_{z>TC}$, and the excess metal content of the distribution beyond that threshold. In the model, the cut-grade and the indicator function are co-estimated.

In preparation for grade interpolation using OK, weights were generated by modelling variograms for all modelled variables in each of the estimation domains. After normal-score transformation, the experimental semi-variograms have relatively low γ_0 values (0.1–0.25). All variograms display acceptable structures and provide support for an Inferred Mineral Resource classification.

Hard domain boundaries were set for estimation after reviewing domain contact analysis plots (Figure 7).

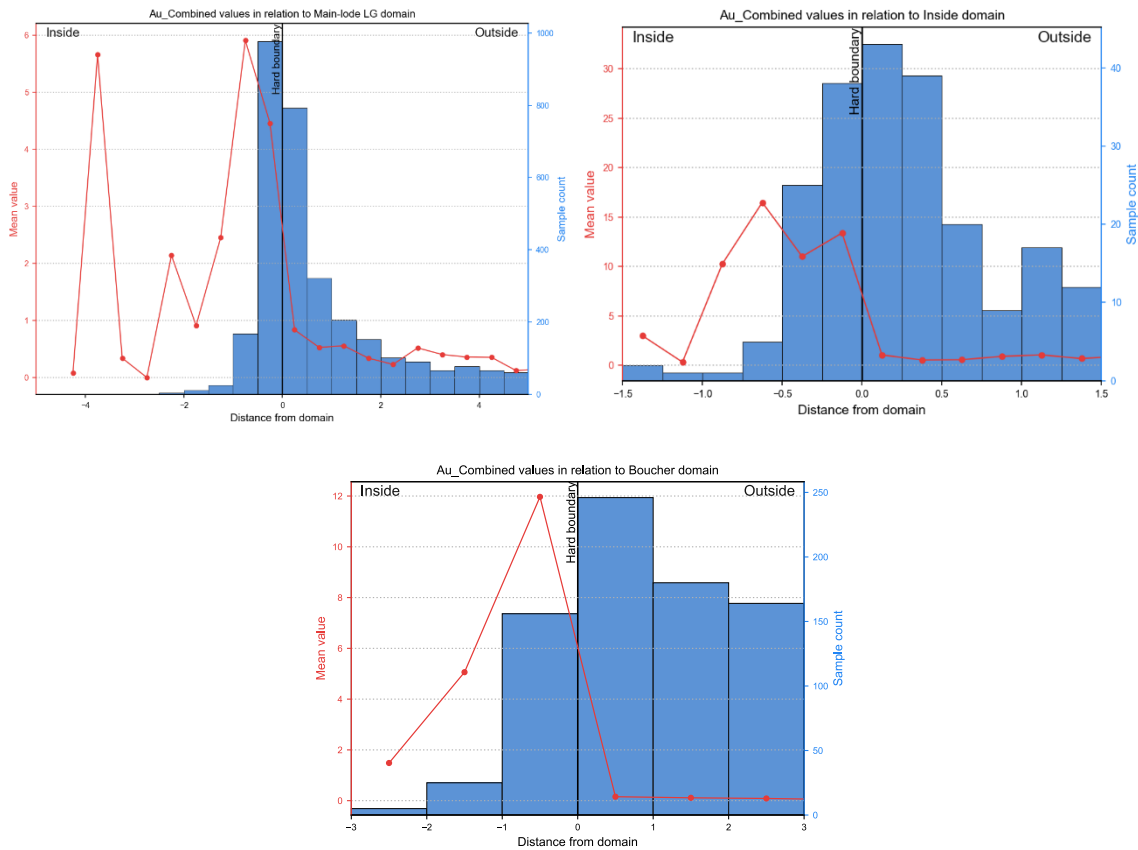


Figure 7 - Contact analysis plots for the Main-lode LG (top left), Main-lode HG (top right) and Boucher (bottom) estimation domains.

A parent block size of 20 m x 3 m x 20 m, sub-blocked to 1 m x 1 m x 1 m (x-y-z), was selected for estimation based on the current drill spacing and estimation vein geometries.

Estimation was completed in three passes using search neighbourhood parameters supported by KNA. Variable orientations were utilised to guide the search ellipse within the estimation domains. The grade of each block was estimated using a minimum of ten and a maximum of 50 samples for passes one and two and a minimum of 8 and a maximum of 50 samples for pass three. Discretisation of 5 x 3 x 5 (x-y-z) was applied.

The Competent Person considers the block model to be appropriately estimated based on validation of input and estimated grades through visual assessment, domain grade mean comparisons, and a review of swath plots.



Bulk Density

The densities of 2022 core samples were determined by the conventional wet-dry 'Archimedes' method.

Density values were assessed globally and within each unit of the geological model. A global bulk density value of 2.81 kg/m³, equivalent to the median bulk density value, was assigned to the in-situ resource due to the low sample support within each unit.

RESOURCE CLASSIFICATION CRITERIA

The Competent person has classified an Inferred Mineral Resource of approximately 3 Mt @ 5.0 g/t Au for 500,000 oz, reported at a cut-off of 3 g/t.m accumulation (Table 1).

The Competent Person has classified the Mineral Resource in the Inferred category in accordance with the JORC Code (2012). Geological evidence is sufficient to imply but not verify the geological and grade continuity. The Mineral Resource is based on exploration, sampling and assaying information gathered through appropriate techniques from underground exposures and drillholes. The unknown sampling procedures, quality assurance and quality control for drilling completed pre-1986, the overall variable drillhole spacing and the small density dataset with potential bias were key contributors to the Inferred classification.

There is no material classified as Indicated or Measured. It is reasonably expected that the majority of Inferred Mineral Resources could be upgraded to Indicated Mineral Resources with continued exploration. Confidence in the estimate is not sufficient to allow the results of the application of technical and economic parameters to be used for detailed planning in Pre-Feasibility or Feasibility Studies. Caution should be exercised if Inferred Mineral Resources are used to support technical and economic studies such as Scoping Studies.

Portions of the deposit that do not have reasonable prospects for eventual economic extraction (RPEEE) are not included in the Mineral Resource. In assessing the reasonable prospects for eventual economic extraction, the Competent Person has evaluated preliminary mining, metallurgical, economic, environmental, social, and geotechnical parameters. The Mineral Resource reported here and confined to the RPEEE volumes is a realistic inventory of mineralisation which, under assumed and justifiable technical, economic, and developmental conditions, may become economically extractable. The reported Mineral Resource was depleted for historical mining and constrained at depth by the data spacing.

Future work will seek to decrease the drill spacing, improve sampling quality control, validate historical data and obtain representative bulk density data for both the resource and waste components of the model.

Cut-Off Grade

A buffer distance of approximately 80 m around existing drillholes was used as a first-pass constraint to the Mineral Resource. The buffer distance was determined from a review of the geological and grade continuity along strike and at depth. The volumes for reasonable prospects for eventual economic extraction were established on a broad contouring of the estimate at a 3 g/t.m accumulation (grade x vein thickness) threshold within the drilling buffer. In determining the g/t.m cut-off, the Competent Person has evaluated preliminary mining, metallurgical, economic, environmental and geotechnical parameters to establish reasonable prospects for eventual economic extraction. The 3 g/t.m cut-off is based on the consideration that a boundary cut-off grade of 2 g/t and a minimum mineralised width of 1.5 m is suitable to sustain reasonable prospects for eventual economic extraction.



Grade-tonnage data above a cut-off grade of 2 g/t Au and above a minimum mineralised width of 1.5 m is presented in Table 2 and Figure 8. Tonnages were estimated on a dry basis. All Mineral Resource tabulations are exclusive of historical mining voids.

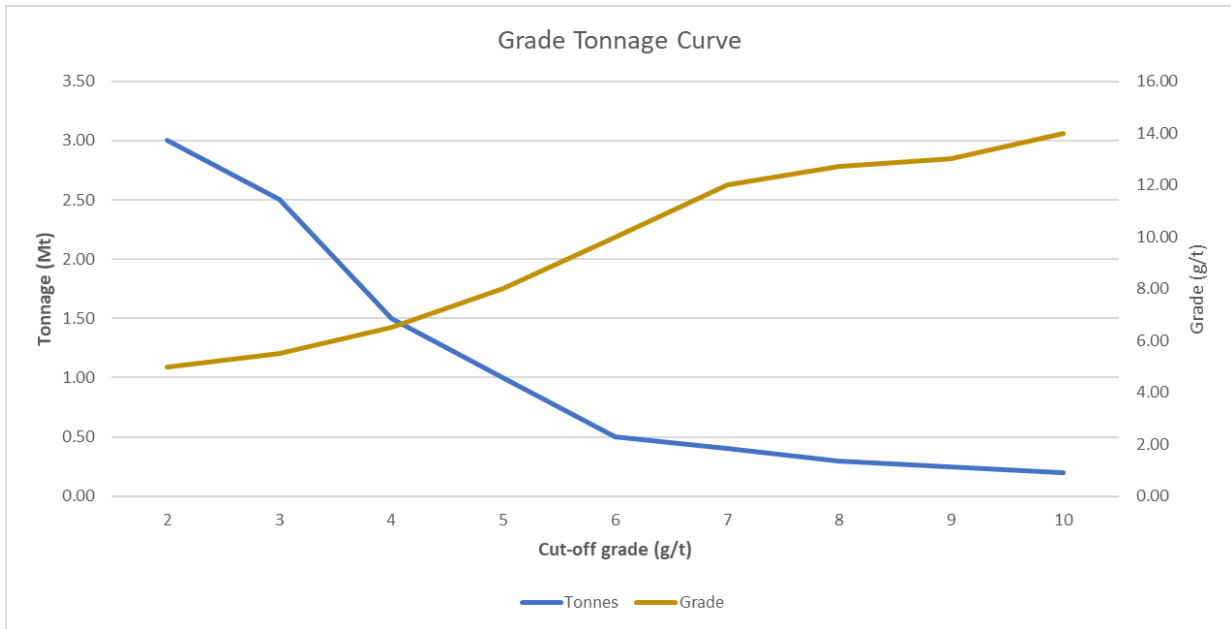


Figure 8 – Grade-tonnage curve for the Labyrinth Inferred Mineral Resource.

MINING AND METALLURGICAL METHODS

The Competent Person has made reasonable assumptions based on a desktop assessment of processing and recovery options to inform the determination of the volumes for reasonable prospects for eventual economic extraction based on an underground mining scenario. No rigorous application has been made (e.g. to establish stope designs). Portions of the deposit that do not have reasonable prospects for eventual economic extraction are not included in the Mineral Resource.

Volumes for reasonable prospects for eventual economic extraction were established on a broad contouring of the estimate at a 3 g/t.m accumulation (grade x vein thickness). The 3 g/t.m cut-off is based on the consideration that a boundary cut-off grade of 2 g/t and a minimum mineralised width of 1.5 m is suitable to sustain reasonable prospects for eventual economic extraction.

Underground mining was undertaken at the project up until the 1980s. All Mineral Resource tabulations are exclusive of historical mining voids (Figure 9).

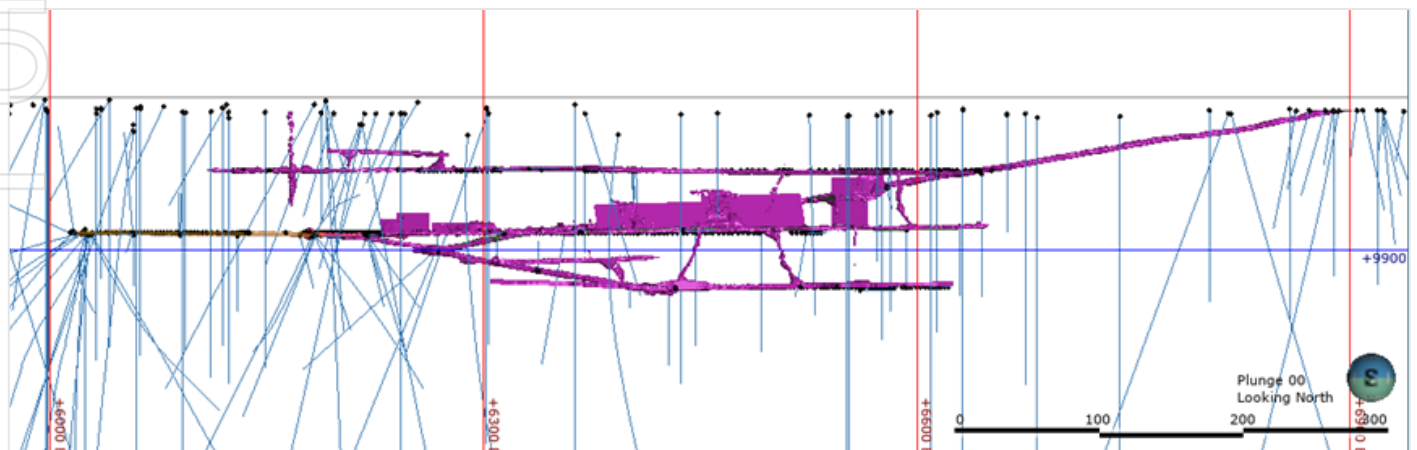


Figure 9 - View to the north presenting the depleted development and production wireframes (magenta).



LABYRINTH EXPLORATION STRATEGY

The exploration and development strategy is to simultaneously carry out resource development work within the known lode extents while exploring the regional potential of the Labyrinth tenure.

The historical shallow drilling results from <100 m below the surface have indicated a strike extension of the McDowell lode of more than 700 m, taking the total strike to over 2.3 km. The next drilling will aim to infill between the Mineral Resource and those mineralised drillholes, decreasing the data spacing to support rapid growth of the Mineral Resource.

The historical results, which sit more than 1,100 m east of the portal, also provide drilling targets for inclusion in the broader regional exploration plan at Labyrinth.

In addition to the significant strike extension possibilities, all lodes are still open at depth which is a major growth target. Interrogation of the resource model will be undertaken to define near-mine high-grade opportunities around the existing five levels of the underground mine.

Regional targets also exist within the Labyrinth tenure with large areas of favourable host rocks and structural settings including the projected intersection of the Hunter Creek and Labyrinth Faults. The Company is in the process of finalising these targets for future exploration.



About Labyrinth Gold Project

The high-grade Labyrinth Gold Project is located in the prolific Abitibi Greenstone Belt and was last mined in the early 1980s until production stopped amid the depressed gold price. Very limited exploration has been conducted on the project since, however, the underground mine remains accessible and includes five main levels of ore drive development to a depth of approximately 130 m below surface.

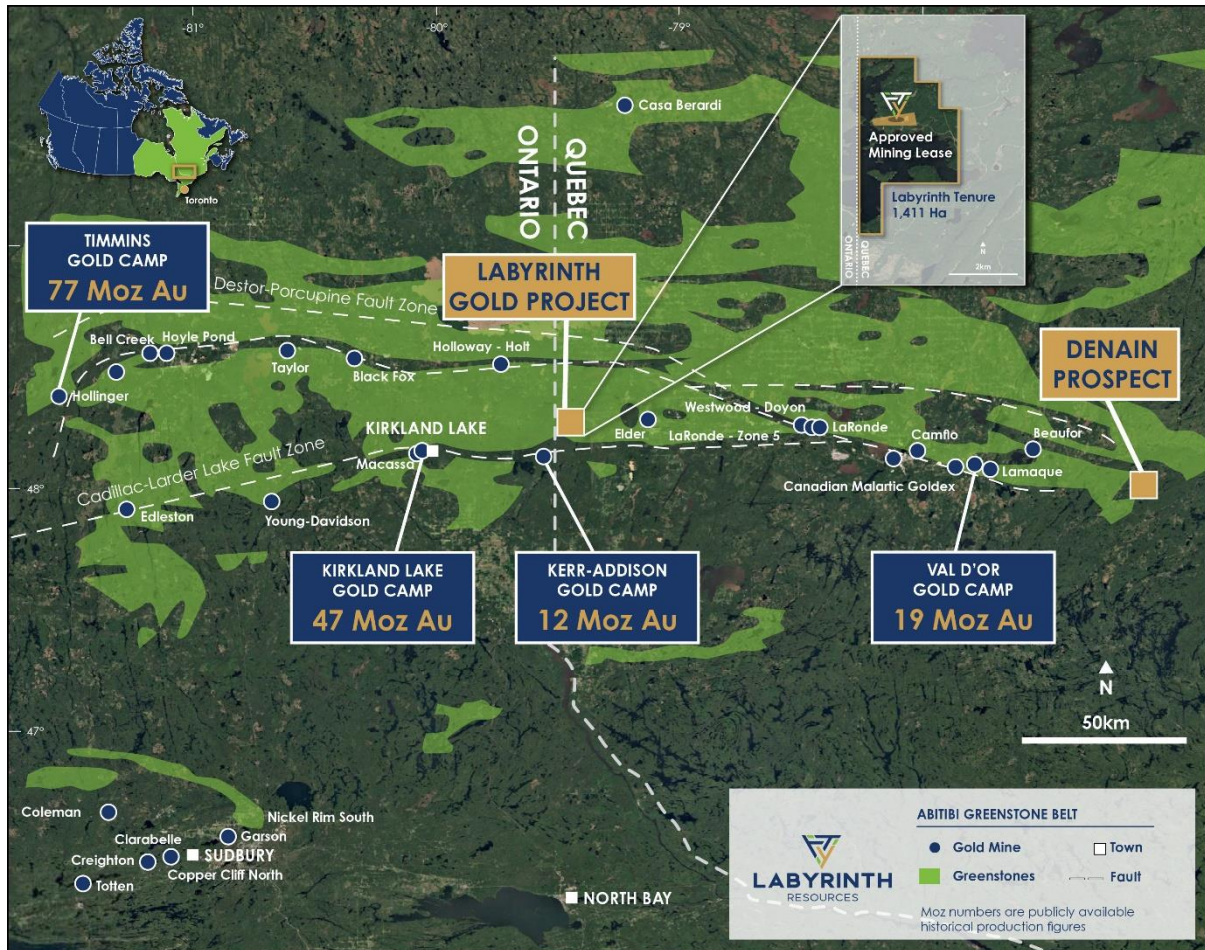


Figure 10 - Location of Labyrinth Resources Projects amongst Abitibi Gold Camps (Sources: Ontario Ministry of Northern Development and Mines Statistics, <https://www.geologyontario.mndm.gov.on.ca>, History of Abitibi Gold Belt (2021) <https://www.visualcapitalist.com/sp/the-history-of-the-abitibi-gold-belt>).

Forward-Looking Information

This announcement contains forward-looking information about the Company and its operations. In certain cases, forward-looking information may be identified by such terms as "anticipates", "believes", "should", "could", "estimates", "target", "likely", "plan", "expects", "may", "intend", "shall", "will", or "would". These statements are based on information currently available to the Company and the Company provides no assurance that actual results will meet management's expectations. Forward-looking statements are subject to risk factors associated with the Company's business, many of which are beyond the control of the Company. It is believed that the expectations reflected in these statements are reasonable but they may be affected by a variety of variables and changes in underlying assumptions which could cause actual results or trends to differ materially from those expressed or implied in such statements. There can be no assurance that actual outcomes will not differ materially from these statements.



Competent Person Statement

The information in this announcement that relates to Exploration Results (metallurgical test work) for the Labyrinth Gold Project is based on information compiled under the supervision of Mr Andrew Chirnside, who is an employee of Labyrinth Resources Limited. Mr Chirnside is a professional geoscientist and Member of the Australian Institute of Mining and Metallurgy and has sufficient experience relevant to the style of mineralisation and type of deposit under consideration, and to the activity which has been undertaken, to qualify as a Competent Person as defined in the 2012 Edition of the Joint Ore Reserves Committee (JORC) Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves. Mr Chirnside consents to the inclusion in this announcement of the matters based on this information in the form and context in which it appears.

The information in this announcement that relates to Mineral Resources is based on information and supporting documentation compiled under the supervision of Mr Rene Sterk, a Competent Person, who is a Fellow and Chartered Professional of The Australasian Institute of Mining and Metallurgy (AusIMM). Mr Sterk is Managing Director of RSC, independent resource development consultants. The full nature of the relationship between Mr Sterk and Labyrinth Resources Limited, including any issue that could be perceived by investors as a conflict of interest, has been disclosed. Mr Sterk has sufficient experience that is relevant to the style of mineralisation and type of deposit under consideration and to the activity which he is undertaking to qualify as a Competent Person as defined in the 2012 Edition of the 'Australasian Code for Reporting of Exploration Results, Mineral Resources and Ore Reserves'.

ASX Announcements referenced in this release

Exploration Results (drillhole intercepts) noted in this release are extracted from the Company's ASX releases dated 24 August 2022, 10 August 2022, 25 July 2022, 7 June 2022, 26 April 2022 and 10 March 2022. The announcements are available to view at <https://labyrinthresources.com/asx-announcements/>. The Company confirms that it is not aware of any new information or data that materially affects the information included in the original market announcements. The Company confirms that the form and context in which the Competent Person's (Mr Andrew Chirnside) findings are presented have not been materially modified from the original market announcement.



APPENDIX 1: JORC CODE, 2012 EDITION – TABLE 1

SECTION 1 SAMPLING TECHNIQUES AND DATA

(Criteria in this section apply to all succeeding sections.)

Criteria	JORC Code explanation	Commentary
Sampling techniques	<ul style="list-style-type: none"> Nature and quality of sampling (eg cut channels, random chips, or specific specialised industry standard measurement tools appropriate to the minerals under investigation, such as down hole gamma sondes, or handheld XRF instruments, etc). These examples should not be taken as limiting the broad meaning of sampling. Include reference to measures taken to ensure sample representivity and the appropriate calibration of any measurement tools or systems used. Aspects of the determination of mineralisation that are Material to the Public Report. In cases where 'industry standard' work has been done this would be relatively simple (eg 'reverse circulation drilling was used to obtain 1 m samples from which 3 kg was pulverised to produce a 30 g charge for fire assay'). In other cases more explanation may be required, such as where there is coarse gold that has inherent sampling problems. Unusual commodities or mineralisation types (eg submarine nodules) may warrant disclosure of detailed information. 	<p>Labyrinth:</p> <ul style="list-style-type: none"> Industry-standard diamond drilling was used to obtain core samples (BQ and NTW), typically 1 m in length but modified to geological boundaries (minimum length of 0.3 m). Whole core (BQ) and half core (NTW) was submitted to SwasLabs for crushing, splitting and pulverisation to produce a 30 g for fire assay with an AAS finish. High-grade samples were reanalysed with a gravimetric finish. Samples containing visible gold were analysed by a screen fire assaying method, consisting of them being sieved after splitting to remove the coarse fraction. Material used in the metallurgical testing was selected from five recent drillholes. Samples were crushed reject from BQ diameter core and a material composite of 40 kg was collected. Individual samples were selected and composited by contract geologists using boundaries of the initial Au assay results. <p>Legacy:</p> <ul style="list-style-type: none"> Diamond drilling was used to obtain core samples (BQ, NQ and ATW), typically 0.5 m in length but modified to geological boundaries. Sampling procedures between 1924 and 1986 are largely unknown, other than that half core was sent for assay. From 2006–2010, half core (NQ) and whole core (BQ and ATW) samples were submitted for analysis by fire assay following crushing, splitting and pulverisation. Samples from 2006–2009 were submitted to Expert Laboratory, Rouyn-Noranda, Quebec for sample preparation and analysis. Whole core samples were crushed, split, pulverised and analysed for gold by Fire Assay using 30 g sample charge with a gravimetric finish. From 2009, half-core samples were sent to SGS Lakefield for crushing, pulverising and analysis by Screen Fire Assay using a 30 g sample charge.
Drilling techniques	<ul style="list-style-type: none"> Drill type (eg core, reverse circulation, open-hole hammer, rotary air blast, auger, Bangka, sonic, etc) and details (eg core diameter, triple or standard tube, depth of diamond tails, face-sampling bit or other type, whether core is oriented and if so, by what method, etc). 	<p>Labyrinth:</p> <ul style="list-style-type: none"> Underground triple-tube diamond drilling using a LM90 diamond drilling rig with wireline core barrel recovery through the inside of the drill string and employing a NTW or BQ size diamond drill bit at the face.



Criteria	JORC Code explanation	Commentary
<p><i>Drill sample recovery</i></p>	<ul style="list-style-type: none"> • <i>Method of recording and assessing core and chip sample recoveries and results assessed.</i> • <i>Measures taken to maximise sample recovery and ensure representative nature of the samples.</i> • <i>Whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.</i> 	<ul style="list-style-type: none"> • Surface diamond drilling using a skid-mounted diamond rig with wireline core barrel recovery through the inside of the drill string and employed an NQ-size diamond drill bit at the face. <p>Legacy:</p> <ul style="list-style-type: none"> • Diamond drilling from surface and underground with various core diameters (BQ, ATW and NQ). <p>Labyrinth:</p> <ul style="list-style-type: none"> • Drill core is assessed for core recovery during drilling operations. Core is meter marked by experienced contract geologists to core blocks inserted by drillers at the end of their runs. • All care is taken to recover the entire core, however, some drilling conditions i.e broken ground can impede 100% recovery. Core recovery of the 2022 underground drill programme was 95%. • There is no known relationship between sample recovery and grade. <p>Legacy:</p> <ul style="list-style-type: none"> • Core recovery records available for drilling between 1924 and 1986 indicate that recovery was variable. Measures taken to maximise recovery are unknown. It is unknown whether a relationship exists between sample recovery and grade. • Core recovery between 2006 and 2009 was recorded in logs by Rocmec geologists and technicians and on average exceeded 90%. Core from 2009–2010 was logged by SGS geologists with stringent procedures.
<p><i>Logging</i></p>	<ul style="list-style-type: none"> • <i>Whether core and chip samples have been geologically and geotechnically logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and metallurgical studies.</i> • <i>Whether logging is qualitative or quantitative in nature. Core (or costean, channel, etc) photography.</i> • <i>The total length and percentage of the relevant intersections logged.</i> 	<p>Labyrinth:</p> <ul style="list-style-type: none"> • All diamond drill core is logged for geology and fundamental geotechnical parameters are taken e.g. RQD, etc. • All core logging is quantitative and a full record is taken by a qualified and experienced contract geologist. <p>Legacy:</p> <ul style="list-style-type: none"> • All drill core samples were geologically logged. Lithology, veining, alteration, mineralisation, sulphide percentage and weathering are all recorded in the geology table of the drill hole database. This logging is quantitative. • Some diamond drill core was geotechnically logged, specifically the most recent campaigns in 2006, 2009 and 2010. This logging is quantitative.



Criteria	JORC Code explanation	Commentary
<p><i>Sub-sampling techniques and sample preparation</i></p>	<ul style="list-style-type: none"> • <i>If core, whether cut or sawn and whether quarter, half or all core taken.</i> • <i>If non-core, whether riffled, tube sampled, rotary split, etc and whether sampled wet or dry.</i> • <i>For all sample types, the nature, quality and appropriateness of the sample preparation technique.</i> • <i>Quality control procedures adopted for all sub-sampling stages to maximise representivity of samples.</i> • <i>Measures taken to ensure that the sampling is representative of the in situ material collected, including for instance results for field duplicate/second-half sampling.</i> • <i>Whether sample sizes are appropriate to the grain size of the material being sampled.</i> 	<p>Labyrinth:</p> <ul style="list-style-type: none"> • NTW core was sawn in half on-site using a diamond table saw, with half retained in trays and the other half sent for assay. One side of the core was consistently taken to ensure no bias is introduced when sampling. Half core NTW samples and whole core BQ samples were sent to SwasLabs for sample preparation: crushed to >80% passing 1700 microns using low chrome steel jaw plates, split using a rotary splitter, pulverised to >85% passing 74 microns, homogenised and split into 30 g pulp samples for assay using a spoon. Samples containing visible gold were sieved after splitting to remove the coarse fraction (as preparation for analysis by screen fire assay). • No duplicates were collected during the sample preparation, however, SwasLabs is an accredited laboratory with industry best practice methods. Internal laboratory QC included the collection of 24 coarse-crush repeat samples daily to check the split quality. Crusher sizing tests are completed by the lab at random between five and eight times per shift. Twenty-four granite flushes are analysed daily to check for contamination of the crusher. Pulveriser sizing tests are completed at random between five and eight times per shift. • Samples sizes are appropriate for the grain size of the material. • Material used in the metallurgical testing was selected from crushed reject of BQ samples. Individual samples were selected by contract geologists. Samples were dried and composited to generate a 40 kg master composite. A 20 kg sub-sample at 300 um K₈₀ was used for the gravity concentration and a 1 kg sub-sample at 20 um P₈₀ was used for the bulk leach test. <p>Legacy:</p> <ul style="list-style-type: none"> • Sub-sampling and preparation procedures between 1924 and 1986 are largely unknown, other than that half core samples, of nominal 0.5 m length, were sent for assay. • Whole-core samples from 2006–2009, with a minimum sample length of 0.15m and maximum sample length of 0.5 m, were sent to Expert Laboratory of Rouyn-Noranda (not certified). Samples were dried and crushed to -1/4 inch with a jaw crusher. Samples were reduced to 90% passing -10 mesh with a rolls crusher. Samples were split using a Jones-type riffle splitter to obtain a 300 g sub-sample which was pulverised to 90% passing -200 mesh using a ring and puck-type pulveriser. A final sample weight of 30 g was weighed out into a crucible. No field duplicates were collected during the sample preparation to ensure representative sampling. A total of 49 pulp duplicate data pairs were available for review. RSC considers the precision and accuracy of the pulp duplicates to be acceptable for classifying an Inferred Mineral Resource. • The Competent Person considers the historical sampling techniques



Criteria	JORC Code explanation	Commentary
<p>Quality of assay data and laboratory tests</p>	<ul style="list-style-type: none"> • <i>The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total.</i> • <i>For geophysical tools, spectrometers, handheld XRF instruments, etc, the parameters used in determining the analysis including instrument make and model, reading times, calibrations factors applied and their derivation, etc.</i> • <i>Nature of quality control procedures adopted (eg standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (ie lack of bias) and precision have been established.</i> 	<ul style="list-style-type: none"> • From 2009–2010, core was sawn in half on site, with half sent to SGS Lakefield for preparation and analysis. Samples were dried before crushing using primary and secondary crushers to achieve 85% passing 10 mesh. The laboratory checks one sample in 50 for % passing at the crushing stage. Samples were then split using a 12-slot, % inch splitter that divides the sample into two portions (pulp and reject). A representative head sample of -150 g was riffled and pulverised to obtain approximately 30 g of 150 mesh from the bulk sample. A total of 19 first-split ½ core duplicate data pairs were available for review. RSC reviewed the available first-split duplicate results and considers their precision and accuracy to be acceptable for classifying an Inferred Mineral Resource. • Samples sizes are considered appropriate for the grain size of the material. <p>Labyrinth:</p> <ul style="list-style-type: none"> • Samples are analysed by fire assay with an AAS finish at SwasLabs. For the samples containing visible gold (with the coarse fraction removed), a weighted average method is used to determine the final assay grade. Samples returning grades >10 g/t Au by AAS finish were reanalysed with a gravimetric finish. • The nature of assaying employed (Fire Assay) is appropriate for the style of mineralisation under review. • Certified Reference Materials and Blanks were inserted at regular intervals 1:20 by qualified contract geologists to ensure a standardized measure of QAQC. RSC's review of CRM performance concluded that any observed bias was low (<2%). Acceptable levels of accuracy and precision have been established. • A lab audit of Swaslabs was undertaken on 1 March 2022 with no deviations from standard practices observed. • Metallurgical testing by gravity concentration and leaching was completed at Baselabs. The 20 kg sub-sample was subjected to gravity concentration. After the gravity concentration is removed, the extraction of gold from the Knelson concentrate was determined by assaying the solution after cyanide leaching (Cyanide Leach: pH 11.0, 50,000ppm NaCN, oxygen sparged, 20,000ppm LeachAid). The 1 kg sub-sample was subjected to a bulk leach extractable gold (BLEG) test (Cyanide Leach: pH 11.0, 5,000ppm NaCN, oxygen sparged, 2000 ppm LeachAid). These methods are in line with industry standards for epithermal gold deposits. <p>Legacy:</p> <ul style="list-style-type: none"> • Analytical procedures between 1924 and 1986 are largely unknown, other than that half-core samples were sent for assay.



Criteria	JORC Code explanation	Commentary
<p>Verification of sampling and assaying</p>	<ul style="list-style-type: none"> • <i>The verification of significant intersections by either independent or alternative company personnel.</i> • <i>The use of twinned holes.</i> • <i>Documentation of primary data, data entry procedures, data verification, data storage (physical and electronic) protocols.</i> • <i>Discuss any adjustment to assay data.</i> 	<ul style="list-style-type: none"> • From 2006–2009, samples were analysed for Au by fire assay with a gravimetric finish at Expert Laboratory (not certified). However, its personnel followed written procedures for the analysis of the samples. Each furnace batch comprised 28 samples, including a laboratory inserted reagent blank and standard. The lower detection limit was 0.03 g/t. All values >3 g/t were verified before reporting. Only laboratory quality control monitoring was used, and the data are unavailable (except for the pulp duplicates discussed in the previous section). • From 2009–2010, samples were analysed for Au by metallic screen fire assay using a 30 g sample charge at SGS Lakefield, an accredited laboratory. Only laboratory quality control monitoring was used, and the data are unavailable (except for the first-split duplicates discussed in the previous section). <p>Labyrinth:</p> <ul style="list-style-type: none"> • Qualified and experienced company geologists design and supervise the drilling program. RSC completed validation of the drilling, sampling and analytical procedures and data to confirm that adequate controls were in place to ensure the data quality is fit for purpose. This validation process included a visit to site and the laboratory to audit drilling and sampling procedures. RSC staff reviewed the project geology, drill core, drill sites, core processing facilities and underground workings to ascertain whether all relevant processes were carried out in accordance with best practice. RSC audited collar locations, core drilling, handling and sampling procedures, observed underground mineral occurrences and verified mineralised intercepts. Sample results in the database were tracked back to core trays, sample bags and metre intervals. • A number of twinned holes are employed during the program to provide a measure of reproducibility and as a measure of spatial variability given the high-grade gold mineralisation present at the property. • Data is entered directly into logging software to minimize any transcription errors. • Metallurgical test results were verified by independent consultants, JT Metallurgical Services. <p>Legacy:</p> <ul style="list-style-type: none"> • In 2007, SGS compiled and verified the contents of the drillhole database. All the information was checked and corroborated with original logs and maps. Only the drillholes with verifiable coordinates were incorporated into the database. • In 2010 SGS verified the database assay table against the paper logs, sections, and location plans for 646 drillhole and channel sample records. SGS verified 3,838 sample assay results. The error rate was less than 1%



Criteria	JORC Code explanation	Commentary
		<p>between paper logs and the database records.</p> <ul style="list-style-type: none"> • SGS converted some assay results from CAD\$/sample and oz/ton to gram/ton to standardize the dataset. This conversion process may have resulted in minor conversion errors for assays accounting for the different units of measure utilized at the time. • A geologist from RSC, on behalf of the Competent Person, visited the site and reviewed the underground workings in relation to several historical drillhole intercepts and verified that the historical data represents the actual deposit and also verified the presence of visible gold in various areas of the mine, including the western extents.
<p><i>Location of data points</i></p>	<ul style="list-style-type: none"> • Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. • Specification of the grid system used. • Quality and adequacy of topographic control. 	<p>Labyrinth:</p> <ul style="list-style-type: none"> • The underground development has been flown by a drone as well as picked up by a surveyor creating high confidence in the topographic control, which drillholes, both historical and recent, are referenced against. • All 2022 drillhole collars are marked out using a hand-held GPS. At the end of each phase of drilling the drillhole collars are also picked up by a qualified surveyor. Downhole survey data were collected using Reflex EZ-trac single shot and Reflex Sprint IQ gyro tool. • In 2007 SGS compiled and verified the contents of the project database. All the information was checked and corroborated with original logs and maps. • SGS extracted historical drillhole information from maps. The maps were digitized and georeferenced with a reliable Georeferencing Information System (GIS). A certain error persists in the historical information ranging from 5–30 m radius. Aberrant drillhole coordinates were corrected and unreliable drillhole information was discarded. When possible, the survey record, assay records, lithological records of the historical drillhole data were verified against the paper logs. If any difference occurred between the coordinates of the paper log and historical digitized collar location map, SGS considered the paper log written information as the most reliable. Downhole deviation data are only available for some holes. • A geologist from RSC, on behalf of the Competent Person, visited the site and verified several recent and historical drillhole collars with a GPS. RSC recommends that all historical collars are surveyed by a professional surveyor. • The grid system in use is a local mine grid that uses the portal as a reference. • The Competent Person considers the topographic control to be adequate to support an Inferred Mineral Resource.
<p><i>Data spacing and distribution</i></p>	<ul style="list-style-type: none"> • Data spacing for reporting of Exploration Results. • Whether the data spacing and distribution is sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and 	<ul style="list-style-type: none"> • Due to the nature of mineralisation and the various drilling and channel sampling campaigns, the hole and sample spacing are highly variable. The drillhole spacing is approximately 40–80 m on average.



Criteria	JORC Code explanation	Commentary
	<p><i>Ore Reserve estimation procedure(s) and classifications applied.</i></p> <ul style="list-style-type: none"> • <i>Whether sample compositing has been applied.</i> 	<ul style="list-style-type: none"> • Data spacing is sufficient to establish geological and grade continuities for Mineral Resource estimation and classification in the Inferred Category (imply but not verify). • No sample compositing was applied.
<p><i>Orientation of data in relation to geological structure</i></p>	<ul style="list-style-type: none"> • <i>Whether the orientation of sampling achieves unbiased sampling of possible structures and the extent to which this is known, considering the deposit type.</i> • <i>If the relationship between the drilling orientation and the orientation of key mineralised structures is considered to have introduced a sampling bias, this should be assessed and reported if material.</i> 	<ul style="list-style-type: none"> • Most drillhole orientations were designed to test perpendicular or near-perpendicular to the orientation of the intersected mineralisation. Drilling was typically oriented perpendicular to the trend and mapped strike and dip of observed mineralisation on surface and elsewhere in the project area. • Due to the density of drilling and the orientation of drilling perpendicular to mineralized bodies, there is limited bias introduced by drillhole orientation.
<p><i>Sample security</i></p>	<ul style="list-style-type: none"> • <i>The measures taken to ensure sample security.</i> 	<p>Labyrinth:</p> <ul style="list-style-type: none"> • The core samples are bagged and sealed with numbered security tags. Once samples arrive at the laboratory, the security tags and corresponding samples are verified against logs. Site is always occupied, and no samples were left at the project during field breaks. <p>Legacy:</p> <ul style="list-style-type: none"> • Security and storage protocols of the historical core pre-2006 are unknown. Core samples from 2006–2010 were bagged in large sample bags and sealed for transport following industry-standard security procedures.
<p><i>Audits or reviews</i></p>	<ul style="list-style-type: none"> • <i>The results of any audits or reviews of sampling techniques and data.</i> 	<ul style="list-style-type: none"> • An audit/review of sampling techniques and data was conducted as part of the 2007 and 2010 NI-43-101 resource estimation by SGS Canada Inc. SGS recommended twin and infill drilling to corroborate historical information and implementing fire assay 30g with metallic screen method. SGS considered the 2006-2008 sampling procedures acceptable. However, SGS recommended implementing robust sampling, logging and core handling procedures in order to certify the traceability, geological interpretation and results of the sampled core. Photography of the entire drill core and completion of downhole deviation surveys were also recommended. • deviation data are only available for some holes. • A geologist from RSC, on behalf of the Competent Person, visited the site in July 2022 to audit/review Labyrinth's sampling techniques and data. Recommendations included resurveying of historical holes by a professional surveyor and the collection of split duplicates. No historical core samples were available for review.



SECTION 2 REPORTING OF EXPLORATION RESULTS

(Criteria listed in the preceding section also apply to this section.)

Criteria	JORC Code explanation	Commentary
Mineral tenement and land tenure status	<ul style="list-style-type: none"> Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. The security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area. 	<ul style="list-style-type: none"> The mineral concessions of the Labyrinth Gold Project consist of 34 unpatented claims and 1 mining lease covering ~1,411Ha. An NSR royalty is payable to Globex of 5% of the first 25,000 ounces produced from the existing BM869 mining lease and 3% for all ounces thereafter. The claims are CDC 2477686 to CDC 2477718. Labyrinth Resources has completed a sale agreement to acquire 100% of the Nippon ownership in the Labyrinth (formerly Rocmec) property, which requires satisfaction of the following considerations: C\$2,000,000 will be paid to Nippon Dragon. 6 months from signing a further C\$1,500,000 will be paid to Nippon Dragon. 12 months from signing a further C\$1,500,000 will be paid. Labyrinth will also pay 4,500 ounces of gold to Nippon over an agreed 48-month period from the Commencement Date and will provide C\$1,085,000 to Nippon for surface exploration at the direction of Labyrinth. Further details are included in ASX release 2 September 2021.
Exploration done by other parties	<ul style="list-style-type: none"> Acknowledgment and appraisal of exploration by other parties. 	<ul style="list-style-type: none"> Since the initial discovery in the 1920s, constant exploration work has been undertaken on the property. Between 1924 and 1986, a total of 23,200 m from 166 historical holes were drilled over the property. Most of the information has been validated from historical paper sections as well as paper logs when possible. Substantial diamond drilling, a 98m shaft, 844m of ramp, 1,729m of underground galleries and 187m of raises were carried out between 1934 and 1983. From 1934–35, Sylvanite Mines drilled 1,111 m on the property. Later, Erie Canadian Mines drilled 10 holes before Bordulac Mines bought the property in 1945. Between November 1946 and September 1947, Bordulac Mines drilled several holes totalling 4,208 m. Core recovery for this program did not exceed 70% and reached hardly 30% locally. A 46m shaft with two (2) compartments was sunk from 1948–49. Approximately 308 m of drifts were dug at level 150 (ft), now called level 45, to explore the Talus vein previously discovered during a surface drilling campaign totalling 2,225 m. Another diamond drilling campaign of 640 m led to the discovery of the McDowell vein. The shaft was deepened to 97.5m depth and an additional 494 m of drift was dug at level 300 (ft), now called level 90, to intercept the McDowell vein. In 1952, underground work was suspended and the mine was flooded. In 1956–57, an electromagnetic survey was carried out to the eastern end of the gold-bearing corridor. From 1961 to 1963, 30 diamond drill holes totalling 7,650 m verified the in-depth extension of the mineral-bearing structures. In 1967, a diamond drilling campaign totalling 2,114 m was conducted to define targets



Criteria	JORC Code explanation	Commentary
		<p>close to surface. In 1969, Gold Hawk Exploration optioned the property and carried out 10 diamond drill holes from surface. In 1972, Gold Hawk Mines bought the mine. It built an access road, pumped out the mine and carried out a sampling program at level 300 (ft), now called level 90. In 1972, Kerr Addison Mines optioned most of the property and carried out a vast ground geophysical survey (magnetic and electromagnetic) in the sectors located apart from the known gold-bearing zones. The same year, Somed Mines of Montreal optioned the remainder of the property and dug a ramp of 134m to extract the Russian Kid vein (original discovery). It also prepared a detailed study of the geological resources in place but decided not to execute its option. In 1978, Explorations El Coco acquired the property and built an all-year access road, set up buildings including offices and a machine shop, and installed compressors and generators. From 1979 to 1981, the company extended the access ramp down to level 425 (ft) now called level 130, totalling 814 m. It also dug 454 m of drifts at level 150 (ft), now called level 45, 202 m at level 300 (ft), now called level 90, and 203 m at level 425 (ft) now called level 130 (m) and prepared six shrinkages at level 300 (ft), now called level 90 (m), for bulk sampling. Bulk sampling was carried out from January 1981 to January 1982. Gold prices dropped to less than USD\$325 during the following months. During this period, 9,366 t of ore was sent to the mill of the Belmoral Mines. At the end of production year 1982, an evaluated quantity of 15,622 t was left on the property of which 4,313 t was on surface. In 1983, Metalor (in joint venture with El Coco) drilled 30 surface diamond drill holes totalling 5,443m and 24 underground diamond drill holes totalling 1,634 m. Also, development work totalling 187 m of raises (levels 150(ft), 300(ft) and Q5), 562 m of drifts (levels 300(ft) and 425(ft)) and the ramp was extended by a further 31m (level 425(ft)). In March 1984, Asselin, Benoit, Boucher, Ducharme, Lapointe, Inc (ABBDL - TECSULT) submitted a feasibility study on the property. Metallurgical tests were carried out at the Centre de recherche minérale du Québec (CRM) in 1984. In 1985, Dassen Gold Resources Ltd. acquired a 90% interest on the property, the 10% remainder belonging to Consolidated Gold Hawk Resources Inc. A diamond drill campaign totalling 4,095 m was carried out to investigate the possible extensions of the known gold-bearing veins.No work was undertaken on the property after 1986.</p> <ul style="list-style-type: none">• Dassen Gold Resources Ltd. had a legal conflict with the lender and the company was sued. Dassen was bankrupted in January 2000 and KPMG Inc was appointed as liquidator at the request of the Royal Bank of Canada. In April 2003, Les entreprises Minières Globex Inc. bought the current property from KPMG Inc. In April 2005, Mirabel Resources Inc. made an agreement with Les entreprises Minières Globex Inc. for an interest of 100% of the Russian Kid property in exchange of cash and shares. In January 2006, Mirabel Resources



Criteria	JORC Code explanation	Commentary
		<p>Inc changed its name to Rocmec Mining Inc.</p> <ul style="list-style-type: none"> From 2006 to 2010 a further 10,300 m of diamond drilling was drilled by Rocmec Mining both on surface and underground on the property. In April 2014, Rocmec Mining Inc changed its name to Nippon Dragon Resources Inc (TSX.V:NIP) focused primarily on developing its proprietary thermal fragmentation mining method (Dragon) using the property as a test bed and demonstration facility.
Geology	<ul style="list-style-type: none"> <i>Deposit type, geological setting and style of mineralisation.</i> 	<ul style="list-style-type: none"> The Labyrinth project is an epithermal gold mineralised system that is hosted in the Archean Abitibi Greenstone belt. Host rocks are predominantly volcanic intrusives ranging from coarse andesites to diorites. Gold mineralisation is hosted within shear zones that have been filled with quartz veining. Mineralisation consists predominantly of pyrite with rare visible gold observed.
Drill hole Information	<ul style="list-style-type: none"> <i>A summary of all information material to the understanding of the exploration results including a tabulation of the following information for all Material drill holes:</i> <ul style="list-style-type: none"> <i>easting and northing of the drill hole collar</i> <i>elevation or RL (Reduced Level – elevation above sea level in metres) of the drill hole collar</i> <i>dip and azimuth of the hole</i> <i>down hole length and interception depth</i> <i>hole length.</i> <i>If the exclusion of this information is justified on the basis that the information is not Material and this exclusion does not detract from the understanding of the report, the Competent Person should clearly explain why this is the case.</i> 	<ul style="list-style-type: none"> All relevant drillhole collar and channel information is provided in Appendix 2. Downhole intercept lengths and depths have been provided in previous public reports by the Company, the latest of which was dated 24 August 2022 and can be accessed at https://labyrinthresources.com/asx-announcements/
Data aggregation methods	<ul style="list-style-type: none"> <i>In reporting Exploration Results, weighting averaging techniques, maximum and/or minimum grade truncations (eg cutting of high grades) and cut-off grades are usually Material and should be stated.</i> <i>Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation should be stated and some typical examples of such aggregations should be shown in detail.</i> <i>The assumptions used for any reporting of metal equivalent values should be clearly stated.</i> 	<ul style="list-style-type: none"> No new Exploration Result intercepts are reported in this report. Figures include intercepts and grades previously reported. Refer to previous public reports by the Company, the latest of which was dated 24 August 2022 and can be accessed at https://labyrinthresources.com/asx-announcements/ No metal equivalents have been used.
Relationship between mineralisation widths and intercept lengths	<ul style="list-style-type: none"> <i>These relationships are particularly important in the reporting of Exploration Results.</i> <i>If the geometry of the mineralisation with respect to the drill hole angle is known, its nature should be reported.</i> <i>If it is not known and only the down hole lengths are reported, there should be a clear statement to this effect (eg ‘down hole length, true width not known’).</i> 	<ul style="list-style-type: none"> The orientation of the gold-bearing structures varies from N070° to N090° with dips ranging between 55° and 80° towards the south. All intersections reported in previous reports are reported downhole lengths only. Most drill holes were drilled as close to orthogonal to the plane of the mineralized lodes as possible. This will vary on an individual basis. It is noted that a few “discovery holes” have intersected the mineralisation at a low angle due to unknown geometry



Criteria	JORC Code explanation	Commentary
		prior to intercepting and this has been accounted for.
<i>Diagrams</i>	<ul style="list-style-type: none"> • <i>Appropriate maps and sections (with scales) and tabulations of intercepts should be included for any significant discovery being reported These should include, but not be limited to a plan view of drill hole collar locations and appropriate sectional views.</i> 	<ul style="list-style-type: none"> • This report and previous announcements contain various maps, figures and sections in the body of the announcement text illustrating the sampling and estimation results in geological context.
<i>Balanced reporting</i>	<ul style="list-style-type: none"> • <i>Where comprehensive reporting of all Exploration Results is not practicable, representative reporting of both low and high grades and/or widths should be practiced to avoid misleading reporting of Exploration Results.</i> 	<ul style="list-style-type: none"> • In the Competent Person's opinion, all material results have been reported in a balanced manner.
<i>Other substantive exploration data</i>	<ul style="list-style-type: none"> • <i>Other exploration data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples – size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.</i> 	<ul style="list-style-type: none"> • No other meaningful substantive exploration data is being reported.
<i>Further work</i>	<ul style="list-style-type: none"> • <i>The nature and scale of planned further work (eg tests for lateral extensions or depth extensions or large-scale step-out drilling).</i> • <i>Diagrams clearly highlighting the areas of possible extensions, including the main geological interpretations and future drilling areas, provided this information is not commercially sensitive.</i> 	<ul style="list-style-type: none"> • Further work will include drilling for depth and lateral extensions. • Completion of further metallurgical testing.



SECTION 3 ESTIMATION AND REPORTING OF MINERAL RESOURCES

(Criteria listed in section 1, and where relevant in section 2, also apply to this section.)

Criteria	JORC Code explanation	Commentary
Database integrity	<ul style="list-style-type: none"> Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes. Data validation procedures used. 	<ul style="list-style-type: none"> Data collected by Labyrinth is entered directly into logging software to minimize any transcription errors. RSC validated the 2022 Labyrinth drilling database in Leapfrog Geo using automatic error identification and further visual checks. Several sample results in the database were also tracked back to assay certificates, core trays, sample bags, metre intervals and geological logs during the site visit. In 2007, SGS compiled and verified the contents of a database of historical results. Most of the information was checked and corroborated with original logs and maps. SGS extracted historical drillhole information from maps.
Site visits	<ul style="list-style-type: none"> Comment on any site visits undertaken by the Competent Person and the outcome of those visits. If no site visits have been undertaken indicate why this is the case. 	<ul style="list-style-type: none"> A geologist from RSC visited the site and SwasLabs in July 2022 on behalf of the Competent Person. The procedures undertaken on-site follow industry standard and in most cases good practice. The procedures undertaken at the SwasLabs follow industry best practices.
Geological interpretation	<ul style="list-style-type: none"> Confidence in (or conversely, the uncertainty of) the geological interpretation of the mineral deposit. Nature of the data used and of any assumptions made. The effect, if any, of alternative interpretations on Mineral Resource estimation. The use of geology in guiding and controlling Mineral Resource estimation. The factors affecting continuity both of grade and geology. 	<ul style="list-style-type: none"> Geological evidence is sufficient to imply but not verify geological and grade continuity. The geological units and mineralised structures have reasonably predictable geometries, supported by an extensive exploration and mining history. A review of gold distributions within the geological domains demonstrates multimodality of gold grades symptomatic of a mixing of grade distributions within each domain. Geological domains are thus not at sufficient resolution to identify grade populations amenable to unbiased estimation. Downhole lithological, structural, and geochemical data, channel samples and legacy level plans were used to aid in constructing the geological model. The Competent Person considers that due to the nature of the deposit, alternative interpretations of the geology are not likely to deviate much from the current model. The basal contact of the overburden unit provided the first-pass constraint on mineralisation, however, resource estimation domains were largely guided by grade data rather than geology. Local-scale variables including rock type, fluid chemistry and pressure give rise to variations in mineralisation assemblage and tenor, structural continuity and alteration intensity.
Dimensions	<ul style="list-style-type: none"> The extent and variability of the Mineral Resource expressed as length (along strike or otherwise), plan width, and depth below surface to the upper and lower limits of the Mineral Resource. 	<ul style="list-style-type: none"> The Mineral Resource extent spans ~2,000 m along strike (085), a width of ~680 m and a thickness of ~600 m. There are width and grade variations in all modelled and estimated structures along strike and down-dip.



Criteria	JORC Code explanation	Commentary
Estimation and modelling techniques	<ul style="list-style-type: none"> • <i>The nature and appropriateness of the estimation technique(s) applied and key assumptions, including treatment of extreme grade values, domaining, interpolation parameters and maximum distance of extrapolation from data points. If a computer assisted estimation method was chosen include a description of computer software and parameters used.</i> • <i>The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate takes appropriate account of such data.</i> • <i>The assumptions made regarding recovery of by-products.</i> • <i>Estimation of deleterious elements or other non-grade variables of economic significance (eg sulphur for acid mine drainage characterisation).</i> • <i>In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed.</i> • <i>Any assumptions behind modelling of selective mining units.</i> • <i>Any assumptions about correlation between variables.</i> • <i>Description of how the geological interpretation was used to control the resource estimates.</i> • <i>Discussion of basis for using or not using grade cutting or capping.</i> • <i>The process of validation, the checking process used, the comparison of model data to drill hole data, and use of reconciliation data if available.</i> 	<ul style="list-style-type: none"> • The depth of mineralisation ranges from surface (0 m) to 600 m. • Six geological domains were created using Leapfrog Geo implicit modelling workflows, based on the downhole geological logging and level plans. Geological domains were not at sufficient resolution to identify grade populations amenable to unbiased estimation. Mineralisation is hosted by faults and fractures and associated with quartz veins. Estimation domains were created implicitly from gold grade data, which are considered to be a proxy for the quartz veining that hosts the mineralisation. Two vein systems were modelled; the Main-lode and Boucher. Wireframes for the estimation domains, representing the quartz veins, were created using an interval selection approach in Leapfrog Edge based on Au grade and guided by a numeric interpolant model using trends of Au mineralisation observed in the drillholes and level plans to guide the search anisotropy. Wireframes were snapped to mineralised intervals and were typically closed off halfway between a mineralised and an unmineralised interval in a drillhole. Mineralisation of the Boucher and Main-lode system remains open to the east, west and at depth. Estimation domains were extended up to 400 m beyond mineralised intercepts and were not constrained for estimation. The risk of extrapolation was considered in classifying the Mineral Resource by using a buffer of 80 m around existing drillholes. The buffer was determined from a review of geological and grade continuity along strike and at depth. Histograms of the composited grade assay data identified the presence of a bimodal Au grade population in the Main-lode, hence high and low-grade domains were created for the Main-lode. The Main-lode domains display a positively skewed population and this was taken into account when selecting the grade estimation method for the Main-lode domains. • The Au estimation was completed using ordinary kriging (OK) for the Boucher domain and a top-cut with indicator residual methodology adapted to very skewed grade distributions (Rivoirard et al., 2010) for the Main-lode domains. Au grades within the Boucher and Main-lode wireframes domains were estimated separately with the grades of one not influencing the grades of the other. Hard domain boundaries were set for estimation after reviewing domain contact analysis plots. • OK is the most widely used non-biased linear estimation method for grade populations that exhibit reasonable statistical homogeneity within estimation domains. The top-cut with indicator residual method (Rivoirard et al., 2010) splits the OK modelled grade distributions into two parts: the first part is the background distribution, characterised by the grade values cut to the top-cut threshold ('TC') and the second part is the tail of high-grade values characterised by the indicator function at that threshold, $I_{z>TC}$, and the excess metal content of the distribution beyond that threshold. In the model, the cut-



Criteria	JORC Code explanation	Commentary
		<p>grade and the indicator function are co-estimated.</p> <ul style="list-style-type: none"> In preparation for grade interpolation using OK, weights were generated by modeling variograms for all modelled variables in each of the estimation domains. Nugget values inferred from the downhole variograms are relatively low (0.1–0.25). A parent block size of 20 m x 3 m x 20 m, sub-blocked to 1 m x 1 m x 1 m (x-y-z), was selected for estimation based on the current drill spacing and estimation vein geometries. Estimation was completed in three passes using search neighbourhood parameters supported by KNA. Variable orientations were utilised to guide the search ellipse within the estimation domains. The grade of each block was estimated using a minimum of ten and a maximum of 50 samples for passes one and two and a minimum of 8 and a maximum of 50 samples for pass three. Discretisation of 5 x 3 x 5 (x-y-z) was applied. The model was validated through visual validation, mean comparison checks, and review of swath plots. The Competent Person considers the block model to be appropriately estimated with block grades representative (within 15%) of the input data.
Moisture	<ul style="list-style-type: none"> Whether the tonnages are estimated on a dry basis or with natural moisture, and the method of determination of the moisture content. 	<ul style="list-style-type: none"> Tonnages were estimated on an in-situ dry weight basis and moisture was not considered.
Cut-off parameters	<ul style="list-style-type: none"> The basis of the adopted cut-off grade(s) or quality parameters applied. 	<ul style="list-style-type: none"> The Mineral Resource is reported at a cut-off of 3 g/t.m accumulation (grade x vein thickness) within an 80 m drilling buffer. The drilling buffer distance was determined from a review of geological and grade continuity along strike and at depth. In determining the 3 g/t.m cut-off the Competent Person has evaluated preliminary mining, metallurgical, economic, environmental and geotechnical parameters for an assumed underground mining scenario to establish reasonable prospects for eventual economic extraction using a gold price of AUD 2,500/oz.
Mining factors or assumptions	<ul style="list-style-type: none"> Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential mining methods, but the assumptions made regarding mining methods and parameters when estimating Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the mining assumptions made. 	<ul style="list-style-type: none"> The Competent Person engaged a mining engineer to assess reasonable parameters for an underground mining scenario, however, no rigorous application has been made (e.g. to establish stope designs). Historical underground mining was undertaken at the project up until the 1980s. Volumes for reasonable prospects for eventual economic extraction were established on a broad contouring of the estimate at a 3 g/t.m accumulation (grade x vein thickness). The 3 g/t.m cut-off is based on the consideration that a boundary cut-off grade of 2 g/t and a minimum mineralised width of 1.5 m is suitable to sustain reasonable prospects for eventual economic extraction.



Criteria	JORC Code explanation	Commentary
<p><i>Metallurgical factors or assumptions</i></p>	<ul style="list-style-type: none"> <i>The basis for assumptions or predictions regarding metallurgical amenability. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider potential metallurgical methods, but the assumptions regarding metallurgical treatment processes and parameters made when reporting Mineral Resources may not always be rigorous. Where this is the case, this should be reported with an explanation of the basis of the metallurgical assumptions made.</i> 	<ul style="list-style-type: none"> Historical metallurgical testing (1984 bottle roll tests) indicates that conventional gold recovery techniques, including gravity, are appropriate. A 1984 metallurgical study from ABBDLTECSULT reported recoveries of material mined from the Rocmec mine at 94%-96% recovery utilising standard flotation and cyanidation. A Camflo mill report from Rocmec also illustrated 92.5–93.6% recovery from Rocmec mine material. However, pilot plant processing in 2009 only achieved 24.5–72% from feed grades ranging from 2–27 g/t Au. Preliminary metallurgical testing on a bulk composite from the recent 2022 drilling by BLEG recovered 97.1% of a 5.6 g/t feed grade. The result indicates that the Labyrinth gold is not refractory and that leaching a flotation concentrate on-site could be a potential option in future. The Competent Person has used 80% recovery as a reasonable order-of-magnitude assumption to support the potential for eventual economic extraction. A full programme of metallurgical test work is recommended to ensure a good understanding of the recoverable Au and potential processing methods.
<p><i>Environmental factors or assumptions</i></p>	<ul style="list-style-type: none"> <i>Assumptions made regarding possible waste and process residue disposal options. It is always necessary as part of the process of determining reasonable prospects for eventual economic extraction to consider the potential environmental impacts of the mining and processing operation. While at this stage the determination of potential environmental impacts, particularly for a greenfields project, may not always be well advanced, the status of early consideration of these potential environmental impacts should be reported. Where these aspects have not been considered this should be reported with an explanation of the environmental assumptions made.</i> 	<ul style="list-style-type: none"> In 2006 Rocmec Mining contracted Laboratoire LTM Inc of Val D'Or who detailed a report that adding 50 kg of dolomitic material to every ton of ore from the Rocmec mine would be sufficient to neutralise potential acid generation from ore material during transport for processing and exceeded the Ministry's rules and regulations. Rocmec received a Certificate of Authorization to mine and transport ore in July 2007 from MDDEP. As such, the Competent Person is not aware of any major environmental constraints that would negatively impact the potential for eventual economic extraction.
<p><i>Bulk density</i></p>	<ul style="list-style-type: none"> <i>Whether assumed or determined. If assumed, the basis for the assumptions. If determined, the method used, whether wet or dry, the frequency of the measurements, the nature, size and representativeness of the samples.</i> <i>The bulk density for bulk material must have been measured by methods that adequately account for void spaces (vugs, porosity, etc), moisture and differences between rock and alteration zones within the deposit.</i> <i>Discuss assumptions for bulk density estimates used in the evaluation process of the different materials.</i> 	<ul style="list-style-type: none"> Bulk density values were determined for approximately 200 core samples from the 2022 Labyrinth drilling. The density was determined using conventional wet-dry 'Archimedes' methods. The Competent Person has concerns around potential bias in the density data as only long, competent pieces of core were measured and no sealing material, e.g. wax, was used to allow measurement of friable/porous sheared samples. Density values were assessed globally and within geological units. A global bulk density value of 2.81, equivalent to the median bulk density, was assigned to the resource estimate due to the low sample support within each geological unit. In the Competent Person's opinion, this is fit for the purpose of estimating an Inferred Mineral Resource; however, this will need to be improved in future



Criteria	JORC Code explanation	Commentary
<p><i>Classification</i></p>	<ul style="list-style-type: none"> • <i>The basis for the classification of the Mineral Resources into varying confidence categories.</i> • <i>Whether appropriate account has been taken of all relevant factors (ie relative confidence in tonnage/grade estimations, reliability of input data, confidence in continuity of geology and metal values, quality, quantity and distribution of the data).</i> • <i>Whether the result appropriately reflects the Competent Person's view of the deposit.</i> 	<p>resource upgrades.</p> <ul style="list-style-type: none"> • The Competent Person has classified the Mineral Resource in the Inferred category in accordance with the JORC Code (2012). The variable drill spacing (often >60 m) and issues relating to confidence in the legacy drilling results, a lack of historical QC data and a lack of representative bulk density data have limited the Mineral Resource from being classified at a higher level of confidence at the time of reporting. • In the Competent Person's view, appropriate account has been taken of all relevant factors that affect resource classification. • Portions of the deposit that do not have reasonable prospects for eventual economic extraction are not included in the Mineral Resource. In assessing the reasonable prospects, the Competent Person has evaluated preliminary mining, metallurgical, economic and geotechnical parameters.
<p><i>Audits or reviews</i></p>	<ul style="list-style-type: none"> • <i>The results of any audits or reviews of Mineral Resource estimates.</i> 	<ul style="list-style-type: none"> • The Mineral Resource has been internally reviewed.
<p><i>Discussion of relative accuracy/confidence</i></p>	<ul style="list-style-type: none"> • <i>Where appropriate a statement of the relative accuracy and confidence level in the Mineral Resource estimate using an approach or procedure deemed appropriate by the Competent Person. For example, the application of statistical or geostatistical procedures to quantify the relative accuracy of the resource within stated confidence limits, or, if such an approach is not deemed appropriate, a qualitative discussion of the factors that could affect the relative accuracy and confidence of the estimate.</i> • <i>The statement should specify whether it relates to global or local estimates, and, if local, state the relevant tonnages, which should be relevant to technical and economic evaluation. Documentation should include assumptions made and the procedures used.</i> • <i>These statements of relative accuracy and confidence of the estimate should be compared with production data, where available.</i> 	<ul style="list-style-type: none"> • The confidence of the Mineral resource is reflected in the Inferred classification of the deposit which has been based on the drill spacing across recent and historical holes, and sampling and assaying information gathered through various techniques. • The Competent Person considers the block model to be appropriately estimated based on validation of input and estimated grades through visual assessment, domain grade mean comparisons, and a review of swath plots. • The Mineral Resource statement is related to a global estimate of in-situ tonnes and grade. There is potential for uncertainty in local estimations of block grades due to potential subtle variations in the deposit that are not captured in the density of available data. • The estimate has not been compared with production data.



APPENDIX 2: DRILLHOLE AND CHANNEL INFORMATION

Table 5 – Drillhole collar information in local mine grid.

Hole ID	Labyrinth Resources Ltd Drillhole	Year	Easting (m)	Northing (m)	RL (m)	Azimuth (°)	Dip (°)	Hole Length (m)	Hole ID	Labyrinth Resources Ltd Drillhole	Year	Easting (m)	Northing (m)	RL (m)	Azimuth (°)	Dip (°)	Hole Length (m)
LABU-22-01	Y	2022	6023.669	2549.465	9911.69	0	-11	270	NB-17	N	1961	6059.42	2453.03	9997.56	0	-68	257.86
LABU-22-02	Y	2022	6022.827	2549.215	9911.51	340	-11	243	NB-18	N	1961	5996.94	2444.5	9997.26	0	-69	287.43
LABU-22-03	Y	2022	6021.364	2548.998	9911.34	314	-11	265	NB-2	N	1961	6363.31	2497.84	10000	0	-70	301.45
LABU-22-04	Y	2022	6021.432	2548.878	9910.7	314	-30	251	NB-20	N	1961	5964.94	2442.67	9997.26	0	-76	300.23
LABU-22-05	Y	2022	6025.075	2548.811	9910.38	0	-56	292	NB-21	N	1961	5935.98	2389.63	9997.56	0	-70	286.94
LABU-22-06	Y	2022	6026.441	2550.094	9910.4	340	-56	278.85	NB-22	N	1961	6119.16	2506.68	9997.56	0	-70	175.26
LABU-22-07	Y	2022	6026.251	2550.367	9910.53	340	-37	258	NB-23	N	1961	6031.99	2437.79	9997.26	0	-45	245.67
LABU-22-08	Y	2022	6025.049	2549.363	9910.39	295	-45	264	NB-25	N	1961	5904.59	2388.11	9996.95	0	-70	276.45
LABU-22-09	Y	2022	6028.592	2550.282	9910.47	40	-48	401	NB-6	N	1961	6683.35	2549.65	9991.16	0	-62	273.41
LABU-22-10	Y	2022	6027.886	2550.53	9910.93	18	-28	300	NB-7	N	1961	6740.65	2545.08	9991.77	0	-70	291.39
LABU-22-11	Y	2022	6183.202	2622.168	9909.2	169.8	-22	177	RS-01-07	N	2007	6190.69	2680.37	10002.6	6	-68	316.68
LABU-22-12	Y	2022	6183.804	2622.372	9909.18	151.7	-31	210	RS-01-09	N	2009	5942.78	2441.91	9993.4	325	-60	453
LABU-22-13	Y	2022	6181.976	2620.848	9908.68	190.3	-22	214.5	RS-01-10	N	2010	5942.78	2441.91	9993.4	350	-45	221.03
LABU-22-14	Y	2022	6180.748	2625.053	9908.62	305	-65	357	RS-02-07	N	2007	6190.69	2680.37	10002.6	4	-15	233.17
LABU-22-15	Y	2022	6182.806	2641.657	9910.2	5	-9	319.5	RS-02-09	N	2009	5942.78	2442.91	9993.4	325	-45	333
LABU-22-16	Y	2022	6027.164	2549.62	9910.4	296	-69	315	RS-02-10	N	2010	5942.78	2441.91	9993.4	10	-50	428
LABU-22-17	Y	2022	6027.53	2549.65	9910.4	349	-71	300	RS-03-07	N	2007	6190.69	2680.37	10002.6	4	-42	237.74
LABS-22-01	Y	2022	6215.285	2369.276	9986.25	0	-65	45	RS-03-09	N	2009	5942.79	2442.91	9993.4	360	-60	433
LABS-22-01A	Y	2022	6215.55	2368.881	9986.32	0	-65	675	RS-03-10	N	2010	6040.91	2768.93	10003.2	323	-44	104
LABS-22-02	Y	2022	6215.985	2368.89	9986.26	0	-60	696.3	RS-04-07	N	2007	6190.69	2680.37	10002.6	350	-25	263.65
LABS-22-03	Y	2022	6815.602	2414.903	9993.82	0	-60	859	RS-04-09	N	2009	6057.53	2320.95	9986.1	325	-60	560.2
LABS-22-04	Y	2022	6817.518	2413.787	9993.81	0	-70	649	RS-04-10	N	2010	6040.91	2768.93	10003.2	325	-90	171
LABS-22-05	Y	2022	6214.171	2366.703	9986.28	0	-65	223	RS-05-09	N	2009	6182.79	2679.11	10000.2	327	-45	279.56
1	N	1935	6888.02	2678.08	9996.04	345	-59	45.08	RS-05-10	N	2010	5996.25	2736.82	10003.3	330	-44	105
10	N	1935	6967.87	2778.55	10001.3	177	-41	74.98	RS-06-01	N	2006	6057.53	2320.95	9981.54	350	-60	570.6
11	N	1936	6992.51	2794.01	9997.44	180	-42	112.93	RS-06-02	N	2006	6289	2304.76	9978.92	352	-55	702
12	N	1936	7022.84	2806.54	9994.21	172	-47	95.4	RS-06-03	N	2006	6393.13	2309.03	9979.27	343	-60	600
150-10	N	1952	6331.44	2651.63	9955.8	160	0	60.96	RS-06-10	N	2006	5996.25	2736.82	10003.4	322	-75	151
150-11	N	1952	6307.07	2654.66	9955.5	158	0	47.55	RS-07-10	N	2010	5955.72	2710.63	9999.71	320	-44	99
150-9	N	1952	6255.25	2651.6	9954.89	160	0	50.29	RS-08-10	N	2010	5958	2713	10000	325	-75	150.3
21	N	1945	6922.11	2677.12	9996.04	15	-70	99.36	RS-09-10	N	2010	5916.15	2682.41	9998.31	334	-45	110.9
22	N	1945	6922.11	2677.12	9996.04	15	-50	76.81	RS-10-10	N	2010	5916.15	2682.41	9998.21	332	-74	150
23	N	1945	6922.11	2677.12	9996.04	15	-35	153.62	RS-11-10	N	2010	5870.98	2674.32	9997.31	328	-45	93.15
24	N	1945	6908.74	2647.55	9996.04	15	-50	90.22	RS-12-10	N	2010	6122	2827	10000	325	-45	99
25	N	1945	6882.78	2645.09	9996.04	343.5	-45	83.82	RS-13-10	N	2010	6254.43	2892.68	10001.7	329	-42	75
26	N	1945	6871.76	2628.1	9996.04	343.5	-45	77.72	RS-14-10	N	2010	6078.58	2802.18	9998.81	333	-45	75
29	N	1946	5729.63	2591.1	9992.38	3.75	-61	143.87	RU-01-08	N	2008	6266.97	2667.64	9899.65	336	-20	242.62
3	N	1935	6904.69	2685.15	9996.04	345	-62	41.76	RU-02-08	N	2008	6266.97	2667.64	9899.65	336	-45	235.3
30	N	1946	5768.29	2590.01	9992.38	0	-45	96.62	RU-03-08	N	2008	6024.27	2548.27	9914.03	0	0	340.77
300-1	N	1952	6177.99	2656.03	9908.86	157	0	51.82	RU-04-08	N	2008	6024.27	2548.27	9914.03	0	-45	266.39
300-10	N	1952	6313.17	2588.97	9911.3	10	0	47.55	RU-05-08	N	2008	6057.5	2551	9910	0	0	55.6
300-11	N	1952	6314.67	2581.5	9911.3	202	0	24.99	RU-06-08	N	2008	6057.5	2551	9910	0	-45	49.48
300-12	N	1952	6336.01	2654.65	9911.8	20	0	18.29	RU-06-23A	N	2006	6356.3	2649.93	9913.74	350	0	182.88
300-14	N	1952	6438.14	2627.22	9913.44	160	0	65.23	RU-06-24A	N	2006	6356.3	2649.93	9912.83	350	-45	130.15
300-15	N	1952	6382.82	2613.05	9912.52	3	0	28.35	RU-06-30	N	2006	6202.45	2637.62	9908.98	0	0	220.07
300-16	N	1952	6400.8	2617.93	9912.22	358	0	18.29	RU-06-30A	N	2006	6202.45	2637.62	9908.98	0	0	311.96
300-17	N	1952	6433.61	2630.27	9913.13	357	0	13.11	RU-07-08	N	2008	6014.36	2547	9911	315	-40	243.84
300-18	N	1952	6368.02	2598.36	9911.61	351	0	38.4	RU-08-08	N	2008	6014.36	2547	9911	315	18	96.1



Hole ID	Labyrinth Resources Ltd Drillhole	Year	Easting (m)	Northing (m)	RL (m)	Azimuth (°)	Dip (°)	Hole Length (m)	Hole ID	Labyrinth Resources Ltd Drillhole	Year	Easting (m)	Northing (m)	RL (m)	Azimuth (°)	Dip (°)	Hole Length (m)
300-19	N	1952	6218.53	2593.85	9910.69	16	-42	48.16	RU-09-08	N	39639	6017	2543	9912	192	-10	92.36
300-2	N	1952	6179.06	2656.19	9908.86	145	0	43.28	RU-10-08	N	2008	6016	2543	9913	187	40	112.78
300-20	N	1952	6218.68	2592.15	9911.61	30	-65	57	RU-11-08	N	2008	6057	2546	9911	184	0	84.4
300-21	N	1952	6220.16	2593.24	9910.08	43	-65	89	RU-12-09	N	2008	6057	2546	9912	184	40	108.26
300-22	N	1952	6220.16	2593.24	9909.17	43	-44	72.24	RU-13-09	N	2008	6057	2546	9911	184	-11	74.55
300-23	N	1952	6523.48	2653.89	9911.61	173	0	116.43	RU-14-09	N	2008	6090	2548	9910	178	0	100
300-23EX	N	1952	6523.49	2658.38	9914.66	0	0	12.19	RU-15-09	N	2008	6090	2548	9911	178	40	55.11
300-24	N	1952	6523.49	2657.86	9911.61	350	-45	63.49	RU-16-09	N	2008	6089	2552	9911	0	0	66.3
300-25	N	1952	6214.15	2656.18	9911.19	340	0	12.5	RU-17-09	N	2008	6089	2552	9912	0	40	44.2
300-26	N	1952	6214.14	2654.65	9911.19	160	0	9.45	RU-18-09	N	2008	6117	2561	9911	0	40	23
300-27	N	1952	6176.01	2682.09	9911.28	320	0	13.72	TF-83-01	N	1983	6918.96	2635.61	9996.04	0	-60	138.99
300-28	N	1952	6282.69	2581.5	9911	13	0	72.54	TF-83-02	N	1983	6888.48	2623.11	9995.73	0	-60	131.67
300-29	N	1952	6281.14	2581.49	9910.69	0	0	57.91	TF-83-03	N	1983	6858	2626.46	9996.95	0	-60	124.05
300-3	N	1952	6172.96	2657.7	9910.08	250	0	52.43	TF-83-04	N	1983	6093.56	2504.24	9994.82	0	-60	182.58
300-4	N	1952	6172.96	2657.7	9909.47	165	-45	51.21	TF-83-05	N	1983	6858	2626.46	9996.95	0	-76	151.49
300-5	N	1952	6172.96	2618.08	9910.08	180	0	117.65	TF-83-06	N	1983	6035.04	2491.74	9996.95	0	-45	184.1
300-6	N	1952	6218.68	2596.74	9910.08	160	0	25.3	TF-83-07	N	1983	6954.01	2615.79	9994.21	0	-60	261.21
300-6EX	N	1952	6217.92	2633.47	9910.08	160	0	20.12	TF-83-08	N	1983	5998.46	2420.42	9995.43	0	-45	214.58
300-7	N	1952	6243.07	2634.39	9911	90	0	15.24	TF-83-09	N	1983	7018.93	2662.43	9994.21	0	-60	182.88
300-8	N	1952	6230.87	2611.98	9911	38	0	15.24	TF-83-10	N	1983	6062.47	2484.12	9996.95	0	-56	182.88
300-9	N	1952	6313.02	2584.4	9911.3	192	0	15.24	TF-83-11	N	1983	7049.41	2662.43	9992.99	0	-60	187.45
31	N	1946	5693.37	2552.04	9992.08	315	-46	84.12	TF-83-12	N	1983	6123.43	2529.84	9994.82	0	-55	213.66
34	N	1945	7319.47	2746.25	9996.95	343	-47	250.55	TF-83-13	N	1983	6062.47	2514.6	9998.48	0	-45	192.02
35	N	1945	5971.25	2345.22	9993.9	0	-35	191.72	TF-83-14	N	1983	6303.26	2590.8	9993.9	0	-45	152.4
36	N	1945	5971.25	2345.22	9993.9	343	-45	77.72	TF-83-15	N	1983	7110.37	2692.91	9992.99	0	-60	183.79
38	N	1945	5879.59	2336.6	9996.04	330	-45	137.16	TF-83-16	N	1983	6303.26	2590.8	9993.9	0	-65	183.18
4	N	1935	6923.53	2692.3	9994.82	345	-60	37.49	TF-83-17	N	1983	7171.33	2692.91	9992.99	0	-60	166.73
42	N	1948	5842.02	2451.32	9993.29	323	-45	259.38	TF-83-18	N	1983	6303.26	2621.28	9993.9	0	-45	181.36
48	N	1945	7051.69	2210.33	9993.9	0	-60	182.88	TF-83-19	N	1983	6576.06	2702.05	9994.82	0	-90	157.58
5	N	1935	6936.94	2686.56	9995.43	345	-60	40.84	TF-83-20	N	1983	7232.29	2692.91	9992.99	0	-60	184.4
51	N	1948	6236.4	2599.39	9993.9	339	-45	68.58	TF-83-21	N	1983	6187.44	2616.71	9994.21	0	-50	99.67
61	N	1948	7353.62	2325.11	10000	0	-60	209.09	TF-83-22	N	1983	7284.72	2692.91	9992.99	0	-50	182.88
67-1	N	1967	5755.74	2511.51	9992.68	319	-50	206.96	TF-83-23	N	1983	6370.32	2569.46	9993.9	28	-57	150.27
67-2	N	1967	5795.38	2551.83	9992.68	319	-50	57	TF-83-24	N	1983	6552.9	2544.17	9992.68	0	-90	488.59
67-3	N	1968	5997.95	2381.49	9994.82	0	-70	323.09	TF-83-25	N	1983	6461.76	2621.28	9994.21	0	-75	74.68
67-4	N	1968	5875.46	2357.63	9993.29	0	-70	311.51	TF-83-26	N	1983	6111.24	2550.26	9995.12	0	-90	183.79
67-5	N	1968	6091.56	2451.31	9994.82	0	-70	267	TF-83-27	N	1983	6614.16	2602.99	9994.82	0	-50	160.63
67-6	N	1968	6609.68	2488.91	9992.68	0	-60	287.12	TF-83-28	N	1983	6525.46	2564.28	9992.68	2	-50	181.97
67-7	N	1968	6891.93	2608.56	9995.73	350	-45	394.72	TF-83-29	N	1983	6581.55	2629.51	9994.82	0	-70	151.49
67-8	N	1968	6862.45	2601.77	9995.73	350	-45	121.92	TF-83-30	N	1983	6675.12	2593.85	9993.9	0	-63	213.36
67-9	N	1968	6572.33	2500.37	9992.68	0	-60	117.04	TF-83-31	N	1983	6428.23	2628.29	9871.98	0	-45	44.5
68	N	1946	6662.32	2625.85	9993.29	0	-60	94.49	TF-83-32	N	1983	6432.8	2602.38	9873.51	180	0	48.77
7	N	1935	6950.76	2689.73	9995.4	355	-59	46.33	TF-83-33	N	1983	6428.23	2628.29	9871.98	0	0	66.75
71	N	1948	6035.04	2549.96	9997.26	0	-45	76.02	TF-83-34	N	1983	6400.8	2599.64	9873.81	0	-15	56.08
81	N	1961	6242.67	2494.55	9993.9	0	-70	456.59	TF-83-35	N	1983	6428.23	2622.19	9871.98	180	-35	97.23
82	N	1961	6436.36	2566.98	9993.29	0	-70	202.08	TF-83-36	N	1983	6446.52	2634.08	9912.52	0	-65	89.31
83	N	1961	6148.71	2521.91	9994.82	0	-60	206.47	TF-83-37	N	1983	6556.86	2641.09	9875.03	180	-5	53.34
85-01	N	1985	6988.45	2601.47	9993.9	0	-60	255.18	TF-83-38	N	1983	6556.86	2646.58	9875.03	0	0	72.54
85-02	N	1985	7018.93	2601.47	9994.21	0	-60	243.84	TF-83-39	N	1983	6560.82	2648.41	9871.98	30	0	50.6
85-02A	N	1985	7034.17	2601.47	9990.86	0	-60	50.9	TF-83-40	N	1983	6492.24	2646.88	9912.52	0	-66	91.44
85-03	N	1985	7049.41	2601.47	9992.99	0	-60	245.97	TF-83-41	N	1983	6519.06	2683.15	9875.03	0	0	78.94
85-04	N	1985	7110.37	2631.95	9992.99	0	-60	212.99	TF-83-42	N	1983	6537.96	2638.96	9875.03	0	0	48.77
85-05	N	1985	7171.33	2631.95	9992.99	0	-60	242.93	TF-83-43	N	1983	6553.2	2644.75	9875.03	0	-75	65.23
85-06	N	1985	7232.29	2601.47	9992.99	0	-60	213.36	TF-83-44	N	1983	6492.24	2646.88	9912.52	0	-35	106.07

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Hole ID	Labyrinth Resources Ltd Drillhole	Year	Easting (m)	Northing (m)	RL (m)	Azimuth (°)	Dip (°)	Hole Length (m)	Hole ID	Labyrinth Resources Ltd Drillhole	Year	Easting (m)	Northing (m)	RL (m)	Azimuth (°)	Dip (°)	Hole Length (m)
85-07	N	1985	7284.72	2631.95	9993.9	0	-60	235.92	TF-83-45	N	1983	6614.16	2663.95	9951.54	0	-75	112.78
85-08	N	1985	7345.68	2631.95	9996.95	0	-60	224	TF-83-46	N	1983	6592.82	2635	9913.44	0	-40	65.11
85-09	N	1985	7467.6	2692.91	9995.43	0	-60	212.02	TF-83-47	N	1983	6644.64	2673.1	9952.15	0	-25	78.64
85-10	N	1986	6062.47	2456.69	9996.95	0	-55	215.49	TF-83-48	N	1983	6629.4	2649.02	9915.88	0	-40	74.37
85-11	N	1986	6062.47	2503.93	9997.56	0	-55	152.4	TF-83-49	N	1983	6309.36	2653.28	9955.19	180	0	79.55
85-12	N	1986	6031.99	2392.68	9993.9	0	-45	230.73	TF-83-50	N	1983	6339.84	2649.32	9955.19	180	0	51.51
85-13	N	1986	5998.46	2493.26	9995.43	0	-70	199.64	TF-83-51	N	1983	6644.64	2654.81	9915.88	0	-45	68.88
85-14	N	1986	6092.95	2450.59	9994.82	0	-55	204.22	TF-83-52	N	1983	6370.32	2635.3	9955.19	180	0	61.57
85-15	N	1986	7406.64	2692.91	9996.95	0	-60	217.99	TF-83-53	N	1983	6370.32	2637.74	9954.28	0	-60	67.97
85-16	N	1986	7406.64	2631.95	9993.9	0	-60	251.16	TF-83-54	N	1983	6129.53	2560.32	9909.47	0	-75	54.86
85-17	N	1986	7467.6	2631.95	9993.9	0	-60	239.88	TH-07	N	2006	6579.03	2690.18	9942.62	165	0	14.02
85-18	N	1986	6123.43	2392.68	9990.86	0	-50	245.97	TH-08	N	2006	6578.99	2690.32	9943.62	165	47	12.19
CR-1	N	1969	6196.16	2660.86	9993.9	343	-45	100.74	TH-09	N	2006	6579.11	2690.4	9941.91	165	-45	19.81
CR-10	N	1969	6802.41	2554.76	9996.04	0	-45	187.45	TH-10	N	2006	6560.31	2686.3	9938.67	163	0	14.63
CR-2	N	1969	6217.51	2664.8	9993.9	343	-45	152.4	TH-11	N	2006	6560.3	2686.06	9940.21	163	24	14.63
CR-3	N	1969	6225.54	2657.55	9993.9	343	-45	138.23	TH-12	N	2006	6560.35	2686.3	9938.67	163	-25	19.81
CR-4	N	1969	6245.51	2672.8	9993.9	343	-45	137.16	TH-13	N	2006	6542.82	2681.88	9935.91	161	1	19.81
CR-7	N	1969	6302.65	2690.47	9993.9	340	-45	236.52	TH-15	N	2006	6569.56	2684.54	9940.96	161	0	23.47
CR-8	N	1969	7004.38	2696.91	9994.21	340	-45	81.99	TH-16	N	2006	6240.78	2658.16	9955.19	177	0	76.81
CR-9	N	1969	7061.49	2719.34	9994.21	340	-45	106.68	TH-17	N	2006	6294.12	2651.76	9955.5	177	0	54.25
FE-1	N	2006	6405.68	2640.48	9953.98	8	-78	36.27	TH-18	N	2006	6385.56	2642.01	9915.57	166	0	32.92
FE-2	N	2006	6403.24	2640.79	9953.98	8	-78	35.05	TH-19	N	2006	6385.56	2642.01	9916.79	166	45	25.91
FE-2 NQ	N	2006	6403.85	2640.79	9953.98	8	-78	20.27	TH-20	N	2006	6362.7	2636.52	9914.35	166	0	34.44
FE-3	N	2006	6402.93	2640.79	9953.98	8	-78	34.75	TH-21	N	2006	6268.21	2603.91	9898.2	180	0	54.64
M1H-3A	N	2006	6409.33	2640.18	9955.19	340	0	31.09	TH-22	N	2006	6268.21	2603.91	9898.81	180	20	31.39
M1H-3B	N	2006	6399.28	2633.78	9955.19	340	0	31.09	TH-25	N	2006	6309.36	2598.57	9891.03	180	0	36.58
NB-1	N	1961	6302.04	2494.79	9997.56	0	-69	248.11	TH-26	N	2006	6337.71	2594.15	9884.79	180	0	22.86
NB-15	N	1961	6551.68	2540.2	9992.08	0	-70	271.27	TH-27	N	2006	6337.71	2594.15	9885.4	180	63	23.16
NB-16	N	1961	6631.84	2552.09	9996.65	0	-70	290.17	TH-28	N	2006	6309.36	2598.57	9891.49	180	20	42.37

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Table 6 – Historical channel sample information in local mine grid.

Channel ID	Eastling (m)	Northing (m)	RL (m)	Azimuth (°)	Dip (°)	Length (m)	Channel ID	Eastling (m)	Northing (m)	RL (m)	Azimuth (°)	Dip (°)	Length (m)	Channel ID	Eastling (m)	Northing (m)	RL (m)	Azimuth (°)	Dip (°)	Length (m)
ECH-150-1001	6372.76	2638.06	9955	212.76793	0	3.57	ECH-300-1214	6051.56	2551.85	9912	183.29054	0	1.07	ECH-300-2283	6418.26	2624.89	9911.61	159.55265	0	0.46
ECH-150-1002	6374.83	2636.6	9955	218.15071	0	3.17	ECH-300-1215	6054.42	2551.75	9912	189.16274	0	2.74	ECH-300-2284	6419.14	2624.38	9911.61	157.03462	0	0.85
ECH-150-1003	6376.46	2635.65	9955	218.11575	0	3.81	ECH-300-1216	6057.87	2550.51	9912	202.04499	0	1.31	ECH-300-2285	6421.49	2625.69	9911.61	161.31409	0	0.98
ECH-150-1004	6378.29	2633.68	9955	216.80504	0	2.99	ECH-300-1217	6059.9	2549.38	9912	192.10398	0	2.38	ECH-300-2287	6424.56	2626.64	9911.61	160.88031	0	1.25
ECH-150-1005	6387.55	2630.22	9955	179.81391	0	3.69	ECH-300-1218	6062.59	2547.67	9912	180	0	0.34	ECH-300-2289	6424.38	2627.15	9911.61	160.83629	0	0.46
ECH-150-1006	6391.69	2630.52	9955	172.37264	0	2.99	ECH-300-1219	6064.93	2548.68	9912	170.47411	0	2.47	ECH-300-2290	6427.57	2627.46	9911.61	164.24141	0	1.43
ECH-150-1007	6400.09	2637.47	9955	149.75913	0	6.49	ECH-300-1220	6067.52	2548.97	9912	169.48901	0	2.53	ECH-300-2292	6430.89	2628.5	9911.61	164.60067	0	2.38
ECH-150-1008	6404.28	2637.22	9955	150.98965	0	3.87	ECH-300-1221	6070.19	2549.42	9912	176.44999	0	2.32	ECH-300-2295	6433.83	2628.85	9911.61	163.07949	0	1.58
ECH-150-1009	6407.92	2639.44	9955	155.20668	0	3.35	ECH-300-1222	6073.09	2550.04	9912	179.84144	0	1.22	ECH-300-2298	6438.34	2629.72	9911.61	163.77805	0	2.99
ECH-150-1010	6413.04	2641.93	9955	156.03728	0	3.6	ECH-300-1223	6075.8	2550.71	9912	177.17068	0	1.89	ECH-300-2301	6440.97	2636.75	9911.61	204.6001	0	0.67
ECH-150-1011	6417.08	2643.67	9955	158.95999	0	3.44	ECH-300-1224	6078.35	2551.17	9912	176.36944	0	2.93	ECH-300-2302	6441.07	2636.2	9911.61	175.66292	0	8.02
ECH-150-1012	6420.18	2645.08	9955	157.3046	0	3.99	ECH-300-1225	6080.94	2551.14	9912	174.70956	0	1.68	ECH-300-2308	6444.77	2632.95	9911.61	170.09131	0	1.89
ECH-150-1013	6461.58	2654.37	9955	167.03601	0	4.18	ECH-300-1226	6083.76	2552.25	9912	174.91064	0	3.57	ECH-300-2311	6447.44	2634.25	9911.61	169.02395	0	2.8
ECH-150-1014	6465.34	2655.58	9955	151.60108	0	3.93	ECH-300-1227	6086.65	2552.26	9912	177.43162	0	2.38	ECH-300-2313	6450.41	2634.54	9911.61	169.07829	0	2.1
ECH-150-1015	6467.87	2657.93	9955	148.74199	0	4.63	ECH-300-1228	6089.92	2552.79	9912	179.43634	0	2.96	ECH-300-2315	6453.34	2635.42	9911.61	166.19621	0	2.04
ECH-150-1016	6471.82	2659.89	9955	152.58843	0	3.57	ECH-300-1229	6092.4	2552.41	9912	179.30076	0	2.47	ECH-300-2317	6456.44	2637.48	9911.61	163.61334	0	2.65
ECH-150-1017	6477.84	2663.25	9955	170.50374	0	3.87	ECH-300-1230	6094.64	2553.21	9912	179.83361	0	3.2	ECH-300-2319	6458.68	2637.39	9911.61	165.10158	0	2.1
ECH-150-1018	6482.6	2663.79	9955	175.81591	0	3.23	ECH-300-1231	6096.82	2552.5	9912	181.21983	0	1.98	ECH-300-2321	6462.5	2639.56	9911.61	167.25286	0	1.8
ECH-150-1019	6486.24	2664.85	9955	172.28506	0	3.87	ECH-300-1232	6099.62	2552.27	9912	182.76603	0	1.43	ECH-300-2324	6466.24	2639.95	9911.61	167.9397	0	1.95
ECH-150-1020	6490.5	2665.66	9955	174.41567	0	3.99	ECH-300-1233	6102.39	2552.21	9912	183.29653	0	1.43	ECH-300-2326	6469.4	2641.4	9911.61	168.14462	0	1.74
ECH-150-1021	6494.58	2666.06	9955	172.80572	0	3.41	ECH-300-1234	6105.23	2551.34	9912	178.46616	0	1.86	ECH-300-2329	6471.84	2642.15	9911.61	166.20722	0	1.8
ECH-150-1022	6504.46	2668.62	9955	164.26441	0	3.05	ECH-300-1235	6108.36	2553.35	9912	190.25216	0	3.29	ECH-300-2331	6476.26	2643.5	9911.61	168.53813	0	1.16
ECH-150-1023	6506.89	2669.41	9955	159.01658	0	3.93	ECH-300-1239	6115.35	2557.05	9912	134.77609	0	2.44	ECH-300-2333	6479.99	2644.33	9911.61	170.25204	0	4.91
ECH-150-1024	6508.99	2670.16	9955	157.24811	0	3.54	ECH-300-1240	6111.41	2554.62	9912	172.22704	0	0.3	ECH-300-2339	6482.91	2643.48	9911.61	178.50865	0	0.46
ECH-150-1025	6511	2671.16	9955	153.21159	0	3.99	ECH-300-1241	6111.64	2555.1	9912	166.66149	0	0.52	ECH-300-2340	6484.17	2643.43	9911.61	168.35686	0	1.68
ECH-150-1026	6513.28	2672	9955	149.40675	0	2.96	ECH-300-1242	6121.98	2560	9912	128.63588	0	0.43	ECH-300-2341	6487.02	2644.56	9911.61	177.24358	0	0.58
ECH-150-1101	6526.7	2678.04	9955	169.96608	0	3.08	ECH-300-1243	6121.05	2559.02	9912	124.4919	0	0.37	ECH-300-2342	6489.99	2643.21	9911.61	178.82811	0	0.18
ECH-150-1102	6532.48	2679.76	9955	175.33529	0	3.38	ECH-300-1244	6123.59	2560.23	9912	186.11331	0	3.05	ECH-300-2343	6491.34	2644.61	9911.61	167.89018	0	0.3
ECH-150-1103	6536.72	2680.86	9955	177.77124	0	3.57	ECH-300-1245	6126.19	2561.19	9912	179.61123	0	3.11	ECH-300-2344	6497.29	2647.24	9911.61	182.32339	0	0.43
ECH-150-1104	6542.09	2680.22	9955	200.46525	0	3.47	ECH-300-1246	6128.72	2560.95	9912	160.57165	0	1.71	ECH-300-2345	6497.9	2650.21	9911.61	168.70548	0	3.63
ECH-150-1105	6546.56	2680.05	9955	203.0492	0	3.41	ECH-300-1247	6131	2561.98	9912	158.99158	0	1.58	ECH-300-2349	6513.12	2651.58	9911.61	160.98394	0	0.67
ECH-150-1106	6547.58	2680.39	9955	113.50991	0	2.56	ECH-300-1248	6131.65	2564.59	9912	143.10812	0	1.46	ECH-300-2350	6520.26	2655.62	9911.61	162.6674	0	1.71
ECH-150-1107	6549.25	2683.48	9955	155.59224	0	3.38	ECH-300-1249	6133.44	2567.22	9912	145.5174	0	2.04	ECH-300-2352	6522.83	2656.48	9911.61	165.88232	0	2.01
ECH-150-1108	6552.95	2684.12	9955	157.03774	0	2.77	ECH-300-1250	6134.94	2565.05	9912	151.02272	0	1.92	ECH-300-2355	6526.27	2656.68	9911.61	164.24143	0	1.62
ECH-150-1109	6556.26	2684.67	9955	165.03264	0	2.8	ECH-300-1251	6137.06	2566.23	9912	154.02652	0	1.28	ECH-300-2358	6528.53	2659.14	9911.61	160.00172	0	1.19
ECH-150-1111	6562.26	2686.05	9955	163.54182	0	3.08	ECH-300-1252	6132.61	2577.96	9912	134.9771	0	0.37	ECH-300-2360	6531.21	2660.51	9911.61	163.44769	0	0.98
ECH-150-1112	6565.68	2686.25	9955	164.52705	0	2.71	ECH-300-1253	6132.97	2578.58	9912	133.50406	0	0.12	ECH-425-1301	6402.51	2600.23	9874.12	176.87499	0	2.26
ECH-150-1113	6568.16	2687.36	9955	163.75485	0	3.26	ECH-300-1254	6133.53	2579.49	9912	133.54151	0	0.37	ECH-425-1302	6404.96	2600.54	9874.12	175.03905	0	2.71
ECH-150-1114	6570.91	2686.92	9955	166.36244	0	2.1	ECH-300-1255	6137.84	2580.2	9912	134.53997	0	0.24	ECH-425-1303	6407.41	2600.99	9874.12	177.74118	0	2.65
ECH-150-1115	6573.5	2687.64	9955	168.60489	0	2.99	ECH-300-1256	6162.99	2602.32	9912	190.19894	0	1.22	ECH-425-1304	6409.83	2601.52	9874.12	177.35503	0	2.62
ECH-150-1116	6549.53	2679.22	9955	209.18157	0	3.23	ECH-300-2046	6175.66	2620.93	9912	137.96073	0	2.23	ECH-425-1305	6412.21	2601.66	9874.12	179.68133	0	2.68
ECH-150-1117	6551.85	2677.86	9955	209.76546	0	3.05	ECH-300-2048	6177.32	2621.72	9912	138.57862	0	1.55	ECH-425-1306	6414.6	2601.44	9874.12	177.30333	0	2.68
ECH-150-1118	6554.2	2676.63	9955	208.94615	0	3.38	ECH-300-2050	6179.67	2623.77	9912	145.59735	0	1.52	ECH-425-1307	6416.99	2601.89	9874.12	174.04051	0	2.62
ECH-150-1119	6556.65	2675.1	9955	209.40925	0	3.23	ECH-300-2051	6181.71	2625.89	9912	142.39105	0	1.68	ECH-425-1308	6419.44	2601.98	9874.12	175.76023	0	2.29
ECH-150-1120	6559.45	2674.06	9955	206.46956	0	3.72	ECH-300-2052	6183.93	2627.89	9912	142.55568	0	1.8	ECH-425-1309	6421.94	2602	9874.12	170.6577	0	1.86
ECH-150-1121	6562.13	2672.51	9955	206.83802	0	3.08	ECH-300-2054	6186.33	2630.46	9912	157.34413	0	1.65	ECH-425-1310	6424.34	2602.3	9874.12	166.04076	0	2.13
ECH-150-1122	6564.3	2671.15	9955	208.18968	0	3.32	ECH-300-2056	6189.2	2631.32	9912	157.40772	0	1.31	ECH-425-1311	6426.54	2603.55	9874.12	171.37717	0	3.38
ECH-150-1123	6566.38	2670.27	9955	206.26874	0	2.71	ECH-300-2058	6191.89	2632.76	9912	155.64108	0	3.02	ECH-425-1312	6428.97	2605.15	9874.12	177.6571	0	4.66
ECH-150-1124	6568.45	2668.71	9955	208.47424	0	2.83	ECH-300-2061	6194.65	2633.84	9912	156.2852	0	2.13	ECH-425-1313	6431.47	2605.5	9874.12	176.99796	0	3.25
ECH-150-1126	6573.9	2667.1	9955	209.07415	0	2.35	ECH-300-2064	6197.15	2635.38	9912	156.11882	0	2.13	ECH-425-1314	6433.79	2605.82	9874.12	173.10805	0	2.99
ECH-150-1127	6575.98	2665.62	9955	210.70091	0	3.05	ECH-300-2067	6200.05	2636.61	9912	161.55129	0								



Channel ID	Eastings (m)	Northing (m)	RL (m)	Azimuth (°)	Dip (°)	Length (m)	Channel ID	Eastings (m)	Northing (m)	RL (m)	Azimuth (°)	Dip (°)	Length (m)	Channel ID	Eastings (m)	Northing (m)	RL (m)	Azimuth (°)	Dip (°)	Length (m)
ECH-150-1129	6579.7	2662.35	9955	211.59913	0	3.29	ECH-300-2072	6206.96	2638.04	9912	180	0	1.68	ECH-425-1317	6440.87	2607.8	9874.12	172.39933	0	3.54
ECH-150-1130	6581.38	2660.41	9955	209.76541	0	2.87	ECH-300-2074	6209.91	2638.13	9912	177.56118	0	1.46	ECH-425-1318	6443.4	2607.12	9874.12	173.95771	0	2.8
ECH-150-1131	6583.6	2659.27	9955	210.21256	0	2.26	ECH-300-2076	6212.99	2638.19	9912	179.03632	0	1.71	ECH-425-1319	6445.86	2607.43	9874.12	173.68377	0	2.93
ECH-150-1132	6581.24	2654.88	9955	160.23848	0	3.05	ECH-300-2078	6215.72	2638.39	9912	181.03623	0	2.01	ECH-425-1320	6448.38	2607.85	9874.12	174.84786	0	3.32
ECH-150-1133	6585.46	2655.96	9955	162.89883	0	3.6	ECH-300-2080	6219.06	2637.2	9912	203.87833	0	1.58	ECH-425-1321	6450.82	2607.43	9874.12	173.73536	0	2.19
ECH-150-1134	6589.75	2657.52	9955	161.90642	0	3.75	ECH-300-2082	6222.02	2635.5	9912	211.11774	0	1.62	ECH-425-1322	6452.84	2607.71	9874.12	173.15185	0	1.95
ECH-150-1135	6591.68	2656.9	9955	158.38337	0	2.65	ECH-300-2084	6224.74	2634.13	9912	208.23697	0	1.92	ECH-425-1323	6455.14	2608.45	9874.12	172.08619	0	2.99
ECH-150-1136	6594.25	2657.95	9955	162.66053	0	3.05	ECH-300-2086	6227.35	2632.72	9912	191.88317	0	2.74	ECH-425-1324	6457.84	2608.74	9874.12	176.73483	0	2.8
ECH-150-1137	6596.99	2658.56	9955	161.63605	0	2.56	ECH-300-2089	6229.9	2631.21	9912	181.48914	0	1.8	ECH-425-1325	6460.34	2608.9	9874.12	179.42413	0	2.96
ECH-150-1139	6603.01	2660.43	9955	158.30894	0	3.17	ECH-300-2091	6226.41	2628.09	9912	89.265446	0	2.01	ECH-425-1326	6462.81	2609.02	9874.12	179.72943	0	2.9
ECH-150-1140	6606.06	2660.71	9955	158.12957	0	2.23	ECH-300-2094	6226.98	2622.3	9912	88.466792	0	1.31	ECH-425-1328	6467.75	2609.15	9874.12	181.80072	0	2.59
ECH-150-1141	6607.3	2662.16	9955	161.89835	0	3.23	ECH-300-2096	6227.51	2614.09	9912	90	0	1.8	ECH-425-1329	6469.88	2609.53	9874.12	168.50433	0	2.77
ECH-150-1142	6609.69	2662.32	9955	162.19524	0	2.56	ECH-300-2098	6228.76	2606.02	9912	91.45528	0	1.46	ECH-425-1330	6471.76	2610.76	9874.12	158.00431	0	2.62
ECH-150-1143	6611.25	2662.9	9955	163.14684	0	2.44	ECH-300-2101	6228.63	2602.72	9912	90	0	0.79	ECH-425-1331	6473.62	2612.23	9874.12	157.64322	0	3.54
ECH-150-1144	6613.99	2662.26	9955	163.33242	0	1.19	ECH-300-2102	6229.15	2599.67	9912	87.209368	0	1.58	ECH-425-1332	6475.64	2613.79	9874.12	160.02178	0	3.51
ECH-150-1145	6615.63	2662.69	9955	164.70777	0	1.28	ECH-300-2104	6229.67	2595.24	9912	86.822599	0	1.58	ECH-425-1333	6479.91	2613.73	9874.12	159.77944	0	4.88
ECH-150-1146	6617.87	2664.15	9955	165.76305	0	2.56	ECH-300-2106	6235.95	2587.83	9912	182.53188	0	1.77	ECH-425-1334	6482.87	2612.81	9874.12	162.53865	0	2.01
ECH-150-1147	6619.1	2664.25	9955	164.55959	0	2.59	ECH-300-2109	6238.93	2588.23	9912	180.53864	0	1.8	ECH-425-1335	6485.15	2613.43	9874.12	159.14762	0	2.07
ECH-150-1148	6620.84	2664.75	9955	164.7856	0	2.47	ECH-300-2112	6242.05	2586.97	9912	181.6223	0	2.01	ECH-425-1336	6487.4	2614.28	9874.12	157.70337	0	2.19
ECH-150-1149	6621.95	2665.35	9955	163.68916	0	2.71	ECH-300-2115	6244.86	2586.18	9912	181.49944	0	1.49	ECH-425-1401	6491.58	2616.93	9874.12	155.18818	0	2.65
ECH-150-1150	6622.58	2666.52	9955	163.86185	0	3.29	ECH-300-2117	6247.76	2585.78	9912	184.01707	0	1.4	ECH-425-1402	6493.83	2617.66	9874.12	156.71292	0	2.41
ECH-150-1151	6624.71	2666.84	9955	164.91455	0	3.11	ECH-300-2120	6251.02	2585.04	9912	182.65685	0	1.43	ECH-425-1403	6495.8	2618.67	9874.12	155.90711	0	2.59
ECH-150-1152	6627.68	2669.64	9955	89.729576	0	3.38	ECH-300-2123	6253.67	2584.69	9912	183.44515	0	1.62	ECH-425-1404	6498.18	2619.78	9874.12	153.41654	0	2.41
ECH-150-1153	6627.87	2668.55	9955	90.136545	0	3.23	ECH-300-2125	6256.79	2584.07	9912	184.50773	0	1.74	ECH-425-1405	6501.19	2621.47	9874.12	154.65981	0	2.44
ECH-150-1154	6627.45	2667.83	9955	89.269167	0	3.63	ECH-300-2127	6259.82	2584.15	9912	183.18303	0	1.25	ECH-425-1406	6503.58	2623.23	9874.12	154.62288	0	2.29
ECH-150-1155	6627.43	2667.05	9955	89.877491	0	3.6	ECH-300-2129	6262.59	2584.72	9912	183.73484	0	2.32	ECH-425-1407	6505.8	2624.15	9874.12	154.67997	0	2.5
ECH-150-1156	6633.1	2669.3	9955	161.64756	0	3.17	ECH-300-2132	6265.69	2585.39	9912	181.04985	0	1.71	ECH-425-1408	6507.96	2625.2	9874.12	153.67238	0	2.35
ECH-150-1157	6634.1	2669.76	9955	155.34203	0	3.2	ECH-300-2134	6268.65	2585.72	9912	181.93672	0	1.22	ECH-425-1409	6509.87	2626.78	9874.12	153.80192	0	3.14
ECH-150-1159	6637.25	2670.94	9955	156.30087	0	2.5	ECH-300-2136	6271.65	2586.16	9912	184.76699	0	2.35	ECH-425-1410	6512.21	2627.52	9874.12	151.6801	0	2.41
ECH-150-1160	6638.31	2671.52	9955	155.06025	0	1.74	ECH-300-2139	6274.56	2586.3	9912	184.33862	0	3.11	ECH-425-1411	6514.56	2629.06	9874.12	151.73429	0	3.17
ECH-150-1161	6639.86	2671	9955	152.78329	0	1.86	ECH-300-2143	6278.36	2584.54	9912	194.50117	0	2.62	ECH-425-1412	6519.21	2628.02	9874.12	144.44165	0	0.67
ECH-150-1162	6641.02	2671.46	9955	151.56805	0	1.74	ECH-300-2147	6281.41	2584.1	9912	194.04758	0	3.54	ECH-425-1413	6519.17	2634.43	9874.12	146.66808	0	1.37
ECH-150-1163	6642.36	2671.78	9955	159.86054	0	1.13	ECH-300-2152	6283.88	2582.96	9912	193.22977	0	1.43	ECH-425-1414	6520.85	2631.43	9874.12	146.94377	0	3.35
ECH-150-1164	6643.68	2672.88	9955	159.86128	0	2.26	ECH-300-2154	6290	2582.76	9912	181.50885	0	1.83	ECH-425-1415	6521.62	2635.94	9874.12	147.05381	0	3.11
ECH-150-1166	6651.97	2674.56	9955	167.33307	0	3.41	ECH-300-2156	6292.95	2583.74	9912	180	0	0.61	ECH-425-1416	6523.96	2637.76	9874.12	148.2837	0	3.38
ECH-150-2001	6255.73	2653.32	9955	176.42077	0	1.65	ECH-300-2157	6533.51	2661.71	9912	164.65796	0	3.6	ECH-425-1418	6528.54	2639.96	9874.12	156.16165	0	2.68
ECH-150-2003	6258.86	2653.82	9955	177.41877	0	1.98	ECH-300-2161	6524.83	2655.18	9912	158.08022	0	0.58	ECH-425-1419	6524.22	2634.01	9874.12	149.27087	0	4.88
ECH-150-2005	6261.84	2655.07	9955	177.13503	0	1.07	ECH-300-2162	6516.58	2653.07	9912	161.18576	0	0.88	ECH-425-1420	6530.09	2635.57	9874.12	175.99448	0	4.18
ECH-150-2006	6265.01	2655.42	9955	177.32636	0	2.13	ECH-300-2163	6498.47	2650.37	9912	157.77708	0	3.6	ECH-425-1421	6532.86	2635.41	9874.12	171.62162	0	3.38
ECH-150-2010	6267.8	2655.22	9955	178.0879	0	0.82	ECH-300-2195	6184.95	2628.9	9912	137.46719	0	0.76	ECH-425-1422	6535.28	2636.71	9874.12	168.25894	0	3.78
ECH-150-2011	6267.86	2654.17	9955	177.35523	0	1.25	ECH-300-2196	6187.5	2630.56	9912	155.1383	0	0.61	ECH-425-1423	6537.05	2638.95	9874.12	165.24422	0	0.37
ECH-150-2012	6271.14	2655.11	9955	177.24961	0	1.74	ECH-300-2197	6190.36	2631.72	9912	149.96053	0	0.61	ECH-425-1424	6537.41	2639.09	9874.12	161.10075	0	0.58
ECH-150-2015	6273.94	2654.84	9955	176.57294	0	1.77	ECH-300-2198	6193.13	2633.06	9912	156.20061	0	0.76	ECH-425-1425	6537.95	2639.22	9874.12	165.95451	0	0.73
ECH-150-2017	6277.2	2655.66	9955	176.70708	0	0.67	ECH-300-2199	6195.85	2634.43	9912	155.27802	0	0.79	ECH-425-1426	6538.14	2634.43	9874.12	160.80747	0	0.67
ECH-150-2018	6281.04	2655.86	9955	174.08865	0	1.92	ECH-300-2200	6198.48	2636.01	9912	155.81724	0	1.07	ECH-425-1427	6537.73	2634.31	9874.12	160.80747	0	0.73
ECH-150-2021	6283.98	2656.21	9955	174.53835	0	2.83	ECH-300-2201	6201.31	2636.81	9912	170.53058	0	0.76	ECH-425-1428	6536.51	2633.47	9874.12	134.97642	0	0.4
ECH-150-2024	6287.17	2655.19	9955	176.29249	0	1.37	ECH-300-2202	6205.19	2637.3	9912	175.63875	0	1.37	ECH-425-1429	6536.08	2633.13	9874.12	133.42867	0	0.91
ECH-150-2026	6290.26	2654.22	9955	175.4633	0	1.34	ECH-300-2203	6208.09	2637.79	9912	175.72795	0	0.61	ECH-425-1430	6536.6	2630.51	9874.12	219.65168	0	2.13
ECH-150-2028	6293.37	2654.53	9955	175.74552	0	1.16	ECH-300-2204	6211.42	2638.15	9912	175.38737	0	0.76	ECH-425-1431	6539.07	2628.99	9874.12	218.73999	0	3.02
ECH-150-2030	6295.95	2655.64	9955	173.86329	0	0.98	ECH-300-2205	6214.24	2637.94	9912	176.24456	0	0.76	ECH-425-1432	6541.61	2627.53	9874.12	215.8221	0	3.29
ECH-150-2032	6299.12	2656.52	9955	176.27607	0	1.1	ECH-300-2206	6217.06	2636.91	9912	183.41992	0	0.91	ECH-425-1433	6544.07	2623.43	9874.12	223.29546	0	1.95



Channel ID	Eastings (m)	Northing (m)	RL (m)	Azimuth (°)	Dip (°)	Length (m)	Channel ID	Eastings (m)	Northing (m)	RL (m)	Azimuth (°)	Dip (°)	Length (m)	Channel ID	Eastings (m)	Northing (m)	RL (m)	Azimuth (°)	Dip (°)	Length (m)	
ECH-150-2042	6281.48	2631.69	9955	175.07846	0	1.37	ECH-300-2211	6227.58	2631.31	9912	200.93922	0	0.76	ECH-425-1440	6551.66	2595.53	9874.12	157.50463	0	2.28	
ECH-150-2044	6284.83	2631.74	9955	173.8148	0	1.01	ECH-300-2212	6229.19	2630.97	9912	196.2728	0	0.76	ECH-425-1441	6554.09	2596.59	9874.12	153.83244	0	2.5	
ECH-150-2361	6145.32	2672.87	9955	180	0	0.3	ECH-300-2213	6297.26	2584.05	9912	182.08336	0	0.91	ECH-425-1442	6555.23	2598.14	9874.12	142.1682	0	3.96	
ECH-150-2362	6143.47	2672.6	9955	151.58983	0	0.49	ECH-300-2214	6300.74	2585.1	9912	180.53079	0	2.74	ECH-425-1443	6557.53	2599.61	9874.12	140.35226	0	3.41	
ECH-150-2363	6141.5	2671.7	9955	156.78249	0	0.37	ECH-300-2218	6303.67	2584.87	9912	180.32362	0	1.92	ECH-425-1444	6559.72	2600.64	9874.12	138.48012	0	2.44	
ECH-150-2364	6138.67	2670.48	9955	144.07039	0	0.35	ECH-300-2221	6303.82	2582.38	9912	180	0	1.04	ECH-425-1445	6561.31	2602.43	9874.12	136.8917	0	2.65	
ECH-150-2365	6137.61	2669.5	9955	150.66967	0	0.46	ECH-300-2223	6306.37	2585.27	9912	182.52773	0	0.7	ECH-425-1446	6563.56	2603.34	9874.12	130.8044	0	3.47	
ECH-150-2366	6136.27	2667.5	9955	110.36233	0	0.73	ECH-300-2228	6336.21	2590.76	9912	155.85446	0	0.91	ECH-425-1447	6567.32	2606.1	9874.12	128.35885	0	2.56	
ECH-150-2368	6134.6	2662.46	9955	106.37436	0	0.7	ECH-300-2229	6338.9	2591.61	9912	158.0642	0	0.91	ECH-425-1448	6571.59	2607.68	9874.12	152.14279	0	2.87	
ECH-150-2369	6133.69	2661.15	9955	120.94148	0	1.31	ECH-300-2230	6341.48	2593.16	9912	162.23965	0	0.76	ECH-425-1449	6574.12	2609.24	9874.12	154.71476	0	2.9	
ECH-150-2370	6132.95	2660.61	9955	158.94755	0	0.58	ECH-300-2231	6343.27	2593.8	9912	157.46383	0	0.3	ECH-425-1450	6576.65	2611.06	9874.12	156.16987	0	3.63	
ECH-150-2371	6130	2659.72	9955	163.89685	0	1.22	ECH-300-2232	6346.26	2595.67	9912	158.79066	0	1.01	ECH-425-1451	6579.24	2612.55	9874.12	155.99782	0	4.05	
ECH-150-2372	6129.91	2660.51	9955	171.86053	0	0.49	ECH-300-2233	6347.21	2593.77	9912	154.04052	0	0.34	ECH-425-1452	6581.82	2613.37	9874.12	155.85887	0	3.57	
ECH-150-2373	6126.45	2658.96	9955	169.3726	0	0.43	ECH-300-2234	6349.24	2596.14	9912	163.52758	0	1.52	ECH-425-1453	6584.54	2614.81	9874.12	153.21348	0	3.54	
ECH-150-2374	6161.92	2676.77	9955	162.46126	0	0.18	ECH-300-2236	6350.42	2596.69	9912	162.12319	0	1.98	ECH-425-1454	6589.81	2613.66	9874.12	157.15168	0	0.73	
ECH-150-2375	6162.22	2675.99	9955	159.13286	0	0.3	ECH-300-2239	6353.14	2597.03	9912	165.67929	0	2.07	ECH-425-1455	6591	2614.94	9874.12	157.36456	0	0.43	
ECH-150-2376	6160.61	2674.07	9955	156.14281	0	0.49	ECH-300-2242	6355.84	2597.61	9912	163.86093	0	1.55	ECH-425-1456	6589.8	2616.78	9874.12	154.18604	0	1.98	
ECH-150-2377	6158.45	2675.23	9955	156.62702	0	0.46	ECH-300-2244	6359.12	2598.13	9912	163.75226	0	1.4	ECH-425-1457	6592.1	2618.27	9874.12	152.65743	0	2.13	
ECH-150-2378	6157.15	2673.57	9955	150.92464	0	0.64	ECH-300-2246	6361.69	2598.02	9912	168.68266	0	0.3	ECH-425-1458	6594.23	2619.39	9874.12	152.42821	0	2.26	
ECH-150-2379	6154.62	2672.56	9955	156.91274	0	0.4	ECH-300-2247	6362.35	2596.91	9912	168.55746	0	0.46	ECH-425-1459	6596.1	2620.54	9874.12	153.22695	0	3.17	
ECH-150-2380	6151.92	2671.2	9955	176.26629	0	0.3	ECH-300-2248	6365.59	2599.05	9912	168.01619	0	0.3	ECH-425-1460	6599.8	2620.35	9874.12	168.37062	0	3.05	
ECH-150-2381	6149.74	2672.37	9955	201.38588	0	0.49	ECH-300-2249	6366.14	2597.51	9912	173.47231	0	0.46	ECH-425-1461	6602.61	2621.07	9874.12	170.61311	0	2.99	
ECH-150-2382	6140.09	2683.78	9955	142.828	0	0.24	ECH-300-2250	6368.03	2599.32	9912	162.86849	0	1.58	ECH-425-1462	6605.45	2621.31	9874.12	166.50258	0	2.47	
ECH-150-2383	6140.7	2684.96	9955	146.8675	0	0.43	ECH-300-2252	6370.04	2600.61	9912	175.84207	0	1.92	ECH-425-1463	6608.08	2622.16	9874.12	167.23756	0	2.99	
ECH-150-2384	6138.91	2688.39	9955	186.52413	0	0.37	ECH-300-2255	6372.66	2602.33	9912	152.74116	0	0.88	ECH-425-1464	6610.41	2622.81	9874.12	160.50277	0	3.26	
ECH-150-2385	6136.66	2688.42	9955	150.82946	0	0.18	ECH-300-2256	6374.7	2605.33	9912	160.12735	0	0.46	ECH-425-1465	6612.74	2623.44	9874.12	159.27013	0	2.87	
ECH-150-2386	6134.31	2688.23	9955	166.87992	0	0.4	ECH-300-2257	6377.81	2608.97	9912	152.62667	0	0.46	ECH-425-1466	6614.83	2624.99	9874.12	154.47311	0	3.54	
ECH-150-2387	6131.65	2686.04	9955	163.79935	0	0.46	ECH-300-2258	6381	2611.21	9912	158.03533	0	0.46	ECH-425-1467	6617.06	2625.98	9874.12	157.39968	0	3.81	
ECH-150-2388	6129.18	2684.75	9955	132.41471	0	0.3	ECH-300-2259	6382.92	2612.11	9912	154.94537	0	1.13	ECH-425-1468	6619.35	2627.31	9874.12	158.35723	0	3.96	
ECH-150-2389	6126.71	2682.9	9955	131.73746	0	0.24	ECH-300-2261	6384.51	2612.67	9912	152.06858	0	1.25	ECH-425-1469	6621.81	2628.71	9874.12	157.75252	0	3.99	
ECH-300-1201	6013.8	2546.66	9912	169.80054	0	2.38	ECH-300-2263	6387.23	2613.31	9912	164.83388	0	0.82	ECH-425-1470	6568.58	2678.63	9874.12	171.24722	0	2.29	
ECH-300-1202	6013.9	2546.15	9912	170.21335	0	1.4	ECH-300-2265	6389.95	2613.75	9912	169.32733	0	1.04	ECH-425-1471	6571.55	2678.65	9874.12	171.00377	0	1.07	
ECH-300-1203	6017.3	2547.04	9912	167.64513	0	2.1	ECH-300-2267	6392.96	2614.4	9912	165.11415	0	0.79	ECH-425-1472	6574.62	2679.21	9874.12	167.8948	0	0.58	
ECH-300-1204	6021.59	2547.22	9912	169.00075	0	2.99	ECH-300-2269	6395.71	2615.61	9912	164.17997	0	1.13	ECH-425-1473	6574.82	2678.51	9874.12	119.45611	0	0.98	
ECH-300-1205	6024.28	2547.66	9912	169.31932	0	2.13	ECH-300-2271	6398.43	2616.45	9912	166.12885	0	1.07	ECH-425-1474	6576.43	2679.4	9874.12	119.5201	0	0.49	
ECH-300-1206	6029.18	2549.2	9912	169.77779	0	2.32	ECH-300-2273	6401.22	2617.72	9912	161.33123	0	0.82	ECH-425-1475	6579.13	2680.16	9874.12	181.84917	0	0.3	
ECH-300-1207	6032.2	2549.2	9912	170.16545	0	1.1	ECH-300-2275	6403.46	2618.41	9912	163.83195	0	1.65	ECH-425-1476	6582.67	2681.84	9874.12	179.039	0	1.04	
ECH-300-1208	6034.84	2550	9912	166.72575	0	2.07	ECH-300-2277	6406.38	2620.11	9912	173.85115	0	0.46	ECH-425-1477	6585.01	2682.87	9874.12	171.24623	0	1.4	
ECH-300-1209	6037.96	2550.42	9912	173.44135	0	1.31	ECH-300-2278	6406.84	2618.37	9912	176.6956	0	0.24	ECH-425-1478	6580.25	2680.79	9874.12	171.01944	0	0.55	
ECH-300-1210	6040	2551	9912	170.70852	0	2.71	ECH-300-2279	6409.22	2620.67	9912	168.68102	0	0.58	ECH-425-1479	6544.02	2636.37	9874.12	77.912109	0	0.4	
ECH-300-1211	6043.12	2551.88	9912	179.18528	0	2.5	ECH-300-2280	6412.68	2621.68	9912	164.0424	0	0.64	ECH-425-1480	6569.37	2606.55	9874.12	102.3977	0	2.71	
ECH-300-1212	6045.94	2552.37	9912	176.15739	0	3.14	ECH-300-2281	6413.04	2622.52	9912	162.41471	0	0.46	ECH-425-1481	6543.02	2625	9874.12	220.12645	0	0.61	
ECH-300-1213	6048.93	2552.38	9912	181.27776	0	2.74	ECH-300-2282	6416.15	2623.17	9912	157.50466	0	0.73								